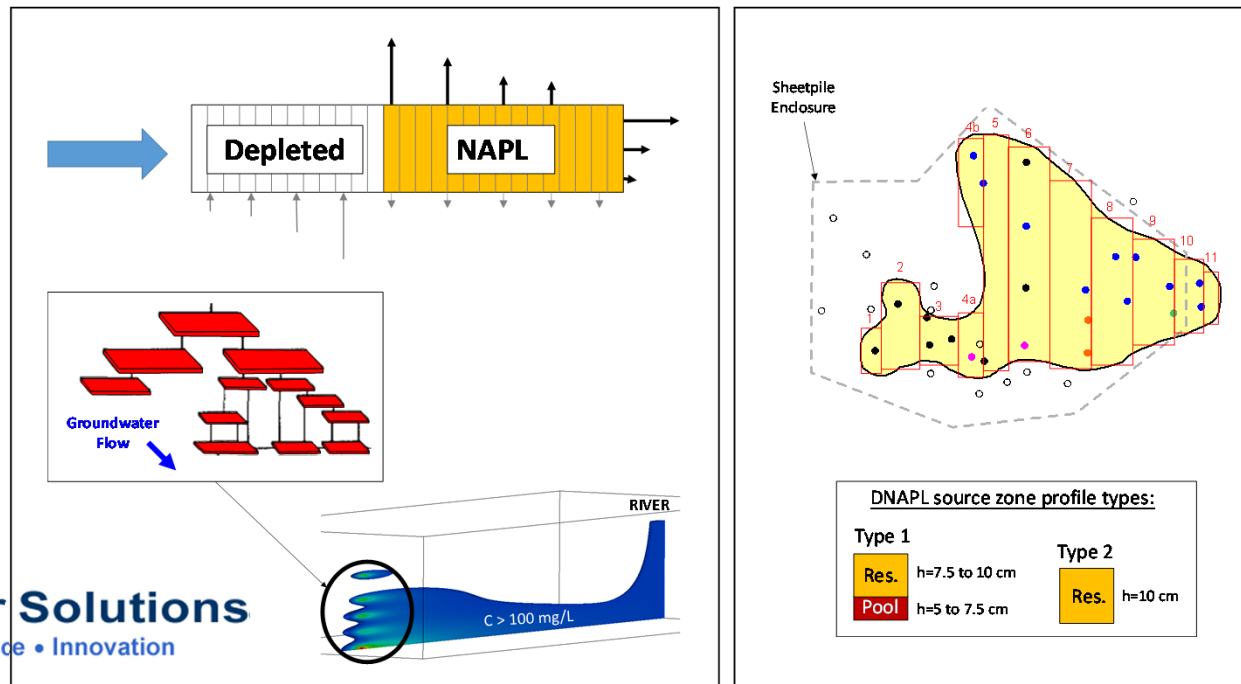


# Modeling DNAPL Depletion for a Well-Characterized Source Zone

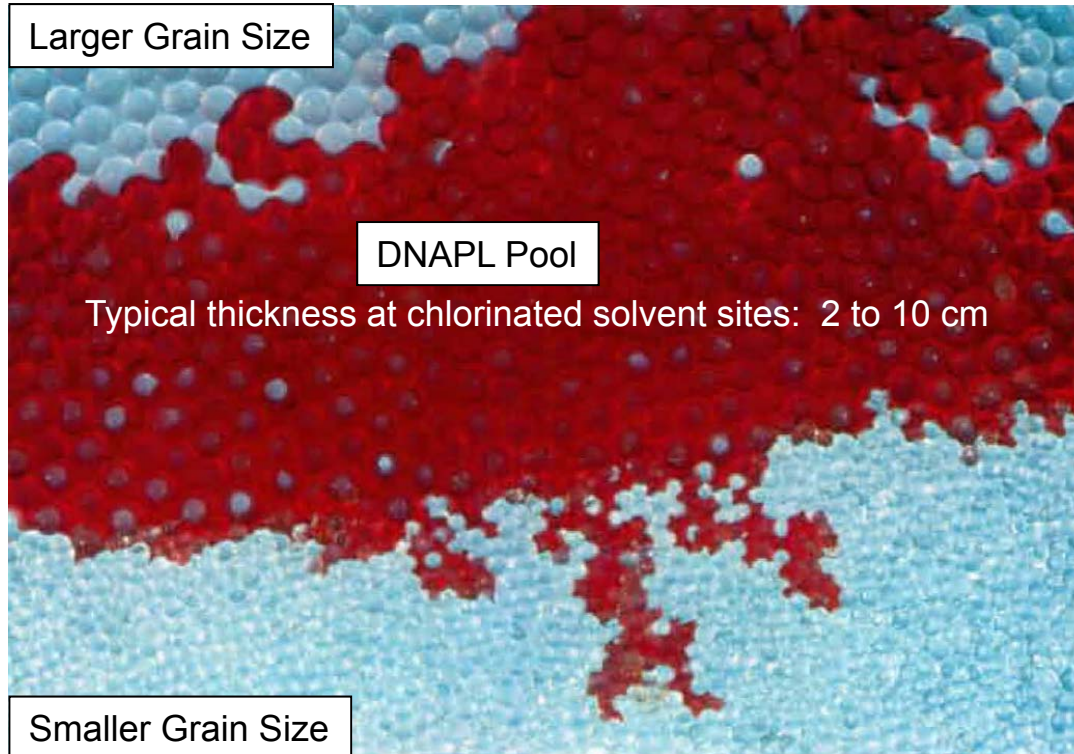
by Grant R. Carey, Ph.D.

Porewater Solutions, Ottawa, Ontario, Canada



**Porewater Solutions**  
Expertise • Experience • Innovation

# NAPL Pool (Free Phase)



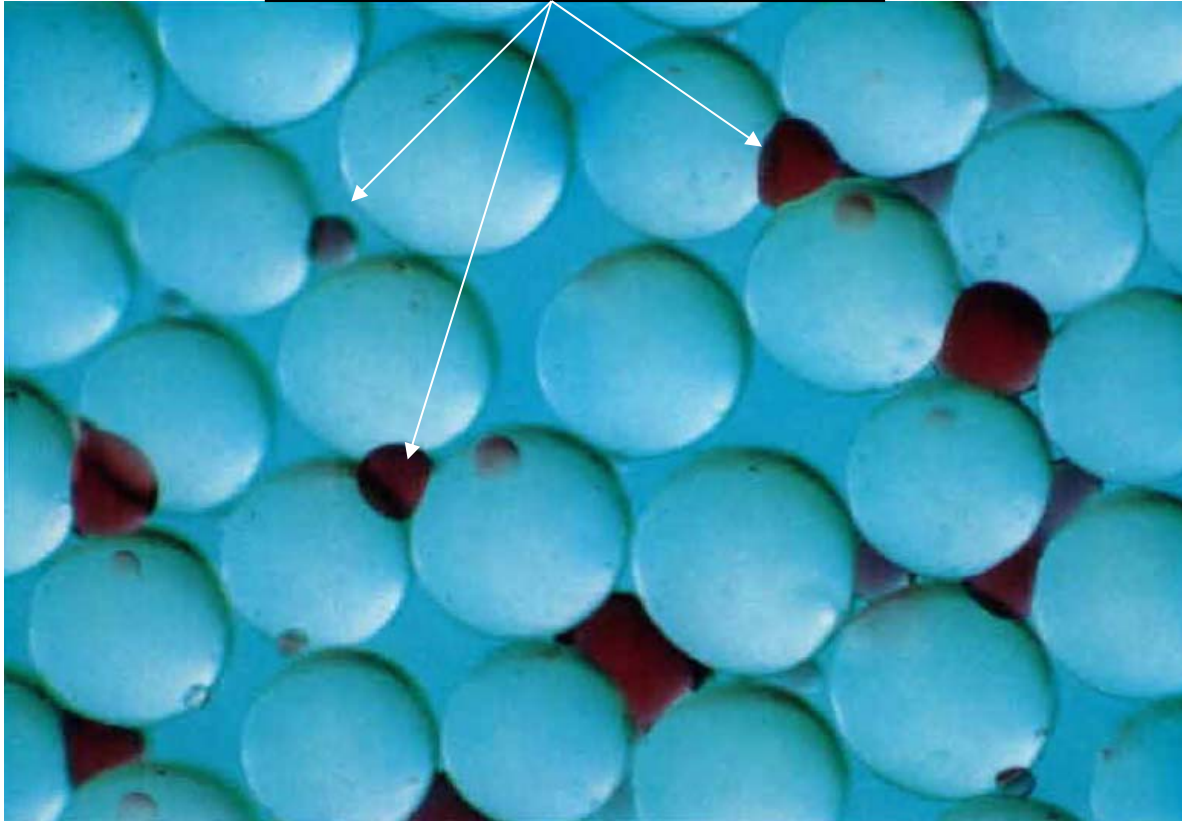
Source: Schwille, 1988

## NAPL Pools

- Above low-K soil
- Horizontal NAPL layer
- Large mass

# Residual NAPL (Ganglia)

DNAPL Ganglia (singlets)



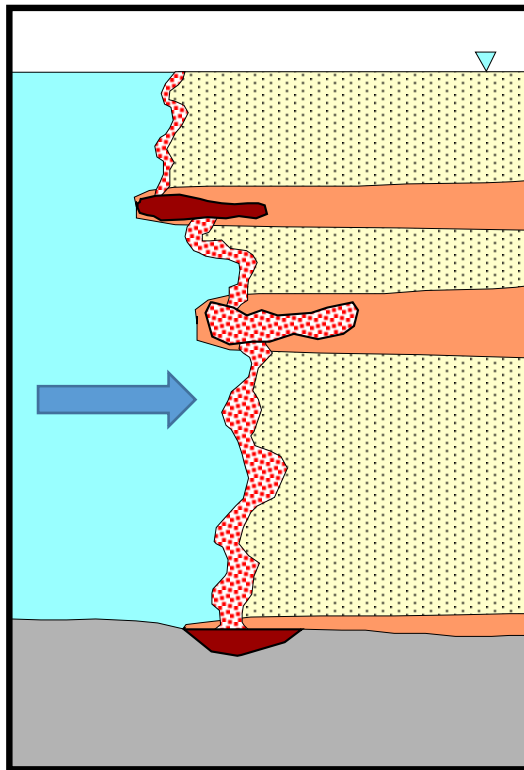
Source: *Schwille, 1988*

## Residual NAPL

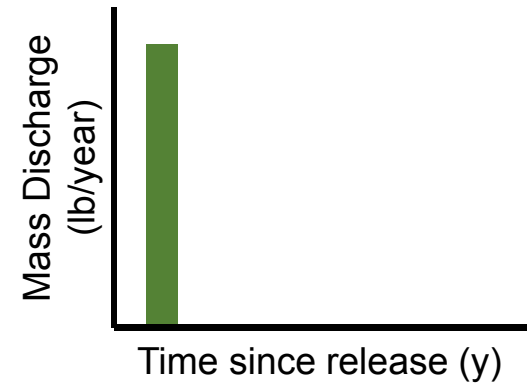
- Small
- Discontinuous
- Immobile

# Mass Discharge Trends

## Fresh Source



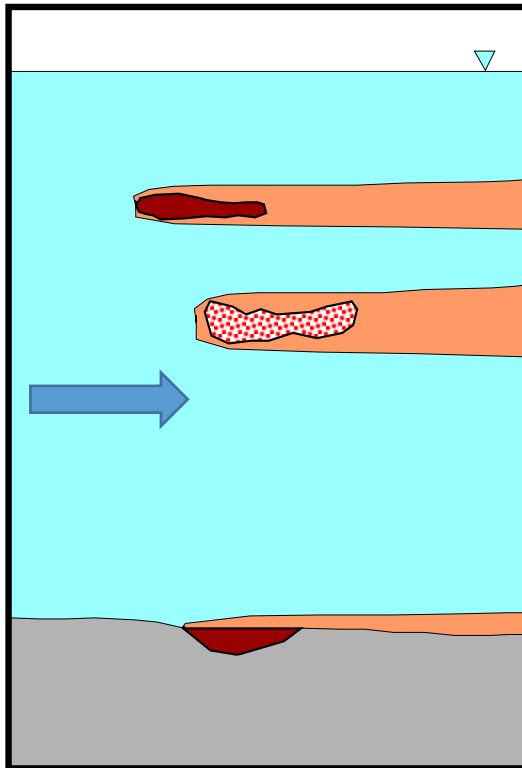
Mass discharge  
from source zone  
(kg/y)



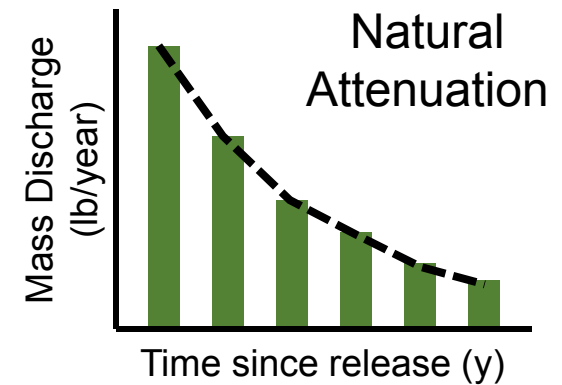
*Modified from Parker et al., 2003*

# Mass Discharge Trends

## Aged Source



Typical source zone mass discharge = 1 to 100 kg/year



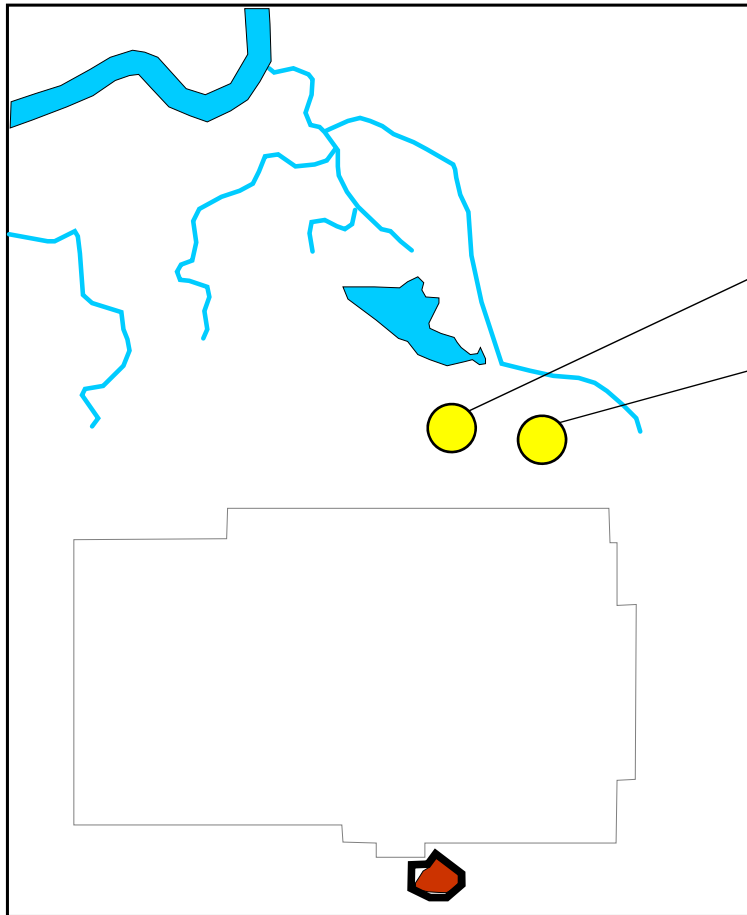
**Newell et al., 2006:**  
Median TCE DNAPL half-life of 6 years

Mass discharge reduction 30x in 30 years

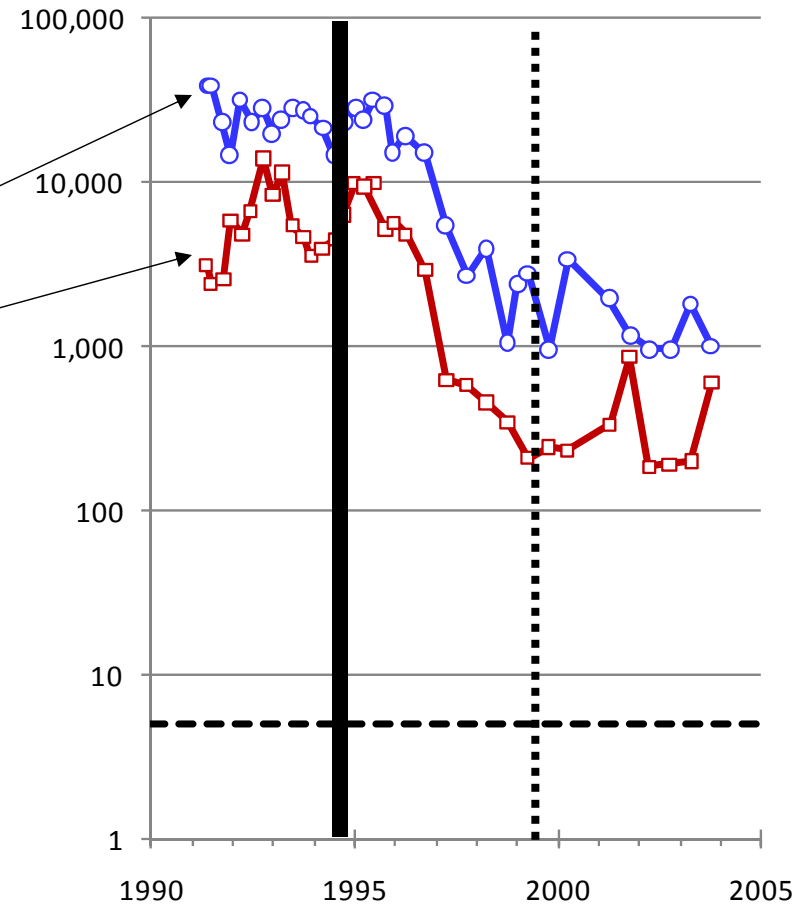
# NAPL Depletion Model Uses

- Compare relative timeframes – natural and enhanced NAPL dissolution alternatives
  - Relative benefit of enhanced diss.
- Improved understanding
- Focus site investigation – key data gaps
- Check CSM – forensic evaluation of NAPL architecture
- Input for plume response model (REMCHLOR, MT3DMS)

# Connecticut Site (Chapman & Parker, 2005)



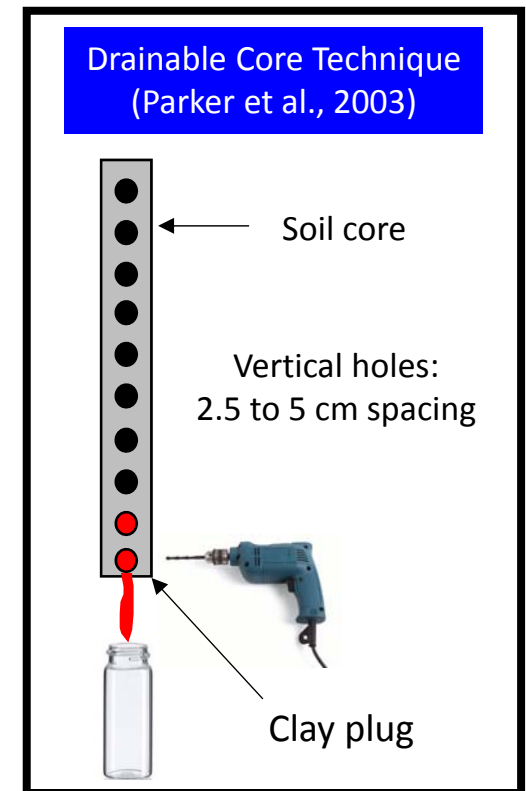
**DNAPL Source Zone**



**Concentration reduction stalled at 93% (15x)**

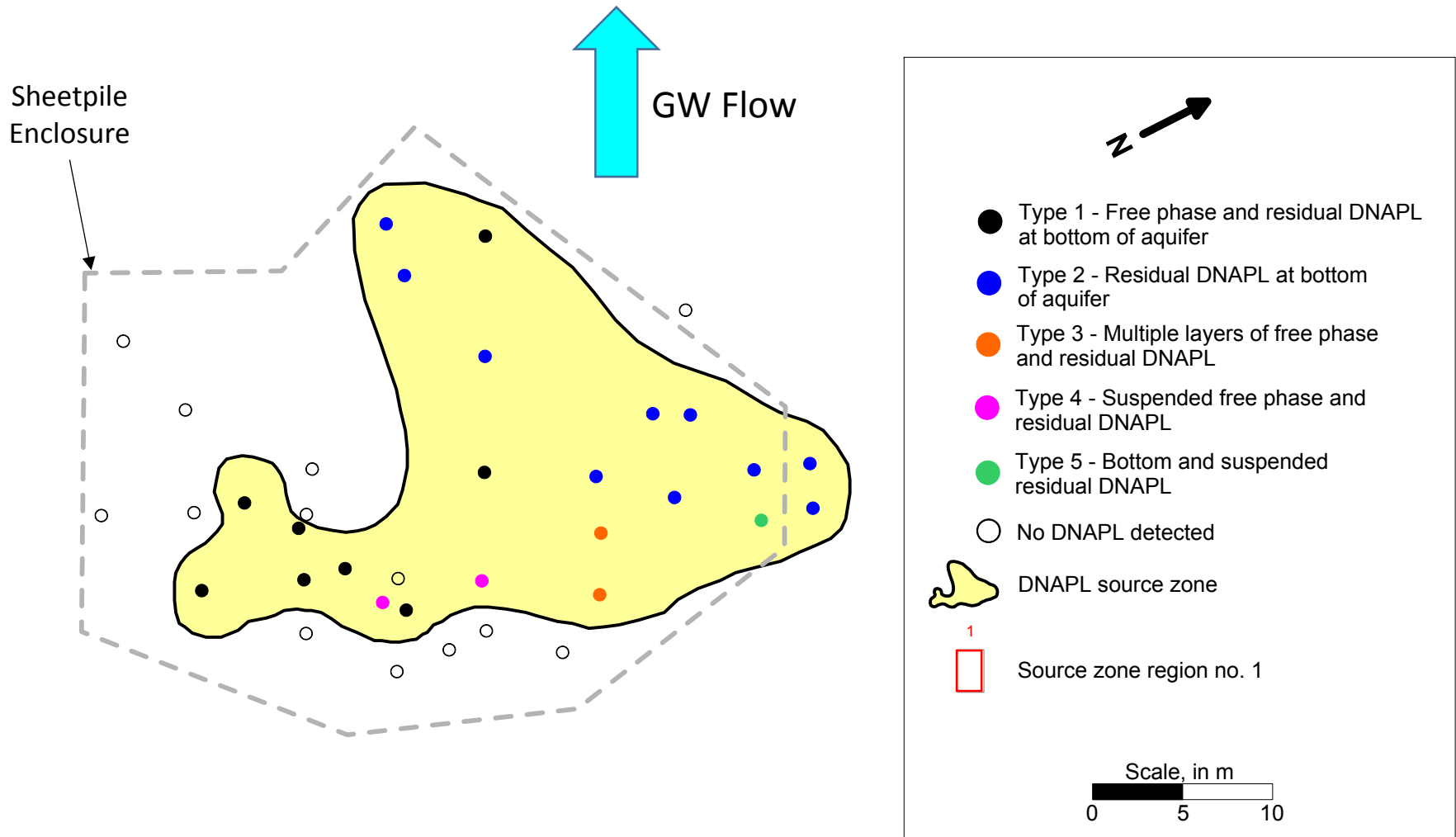
# Case Study: Beth Parker et al. (2003) CT Site

- Connecticut site
- Large DNAPL source zone
  - Bottom of sand aquifer, above aquitard
- Multiple lines of evidence
  - Visual inspection
  - Soil samples – close vertical spacing
    - Partitioning threshold,  $S_n$ , & layer thickness
  - Dye tests (Sudan IV)
  - Drainable core technique → Pool thickness





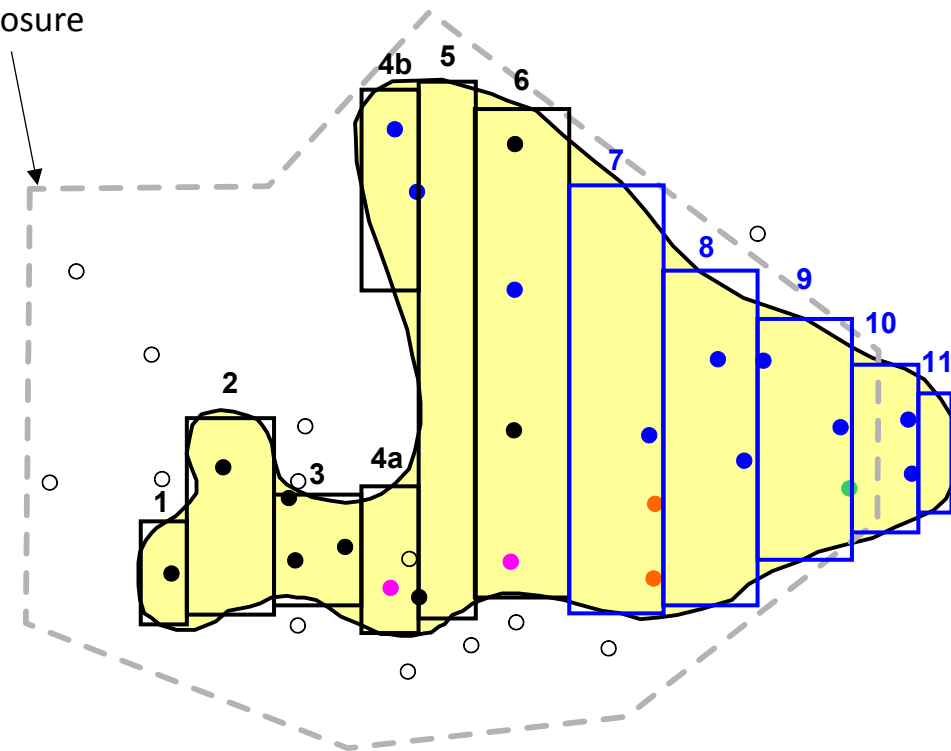
# 1996/97 Source Zone



Data summarized in Stewart (2002) and Parker et al. (2003)

# DNAPL Sub-Zones

Sheetpile Enclosure



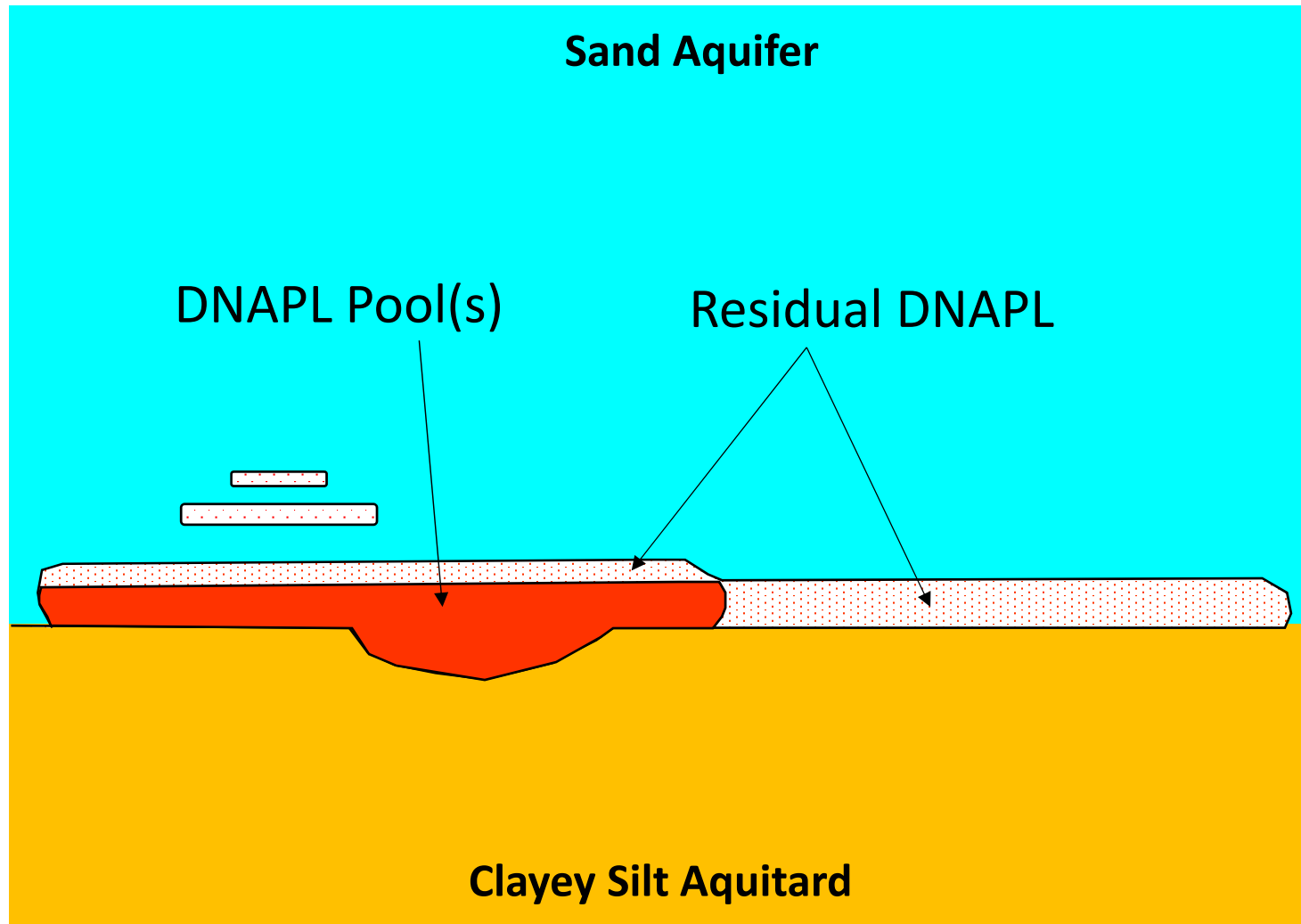
- Type 1 - Free phase and residual DNAPL at bottom of aquifer
- Type 2 - Residual DNAPL at bottom of aquifer
- Type 3 - Multiple layers of free phase and residual DNAPL
- Type 4 - Suspended free phase and residual DNAPL
- Type 5 - Bottom and suspended residual DNAPL
- No DNAPL detected
- DNAPL source zone
- 1 Source zone region no. 1

Scale, in m

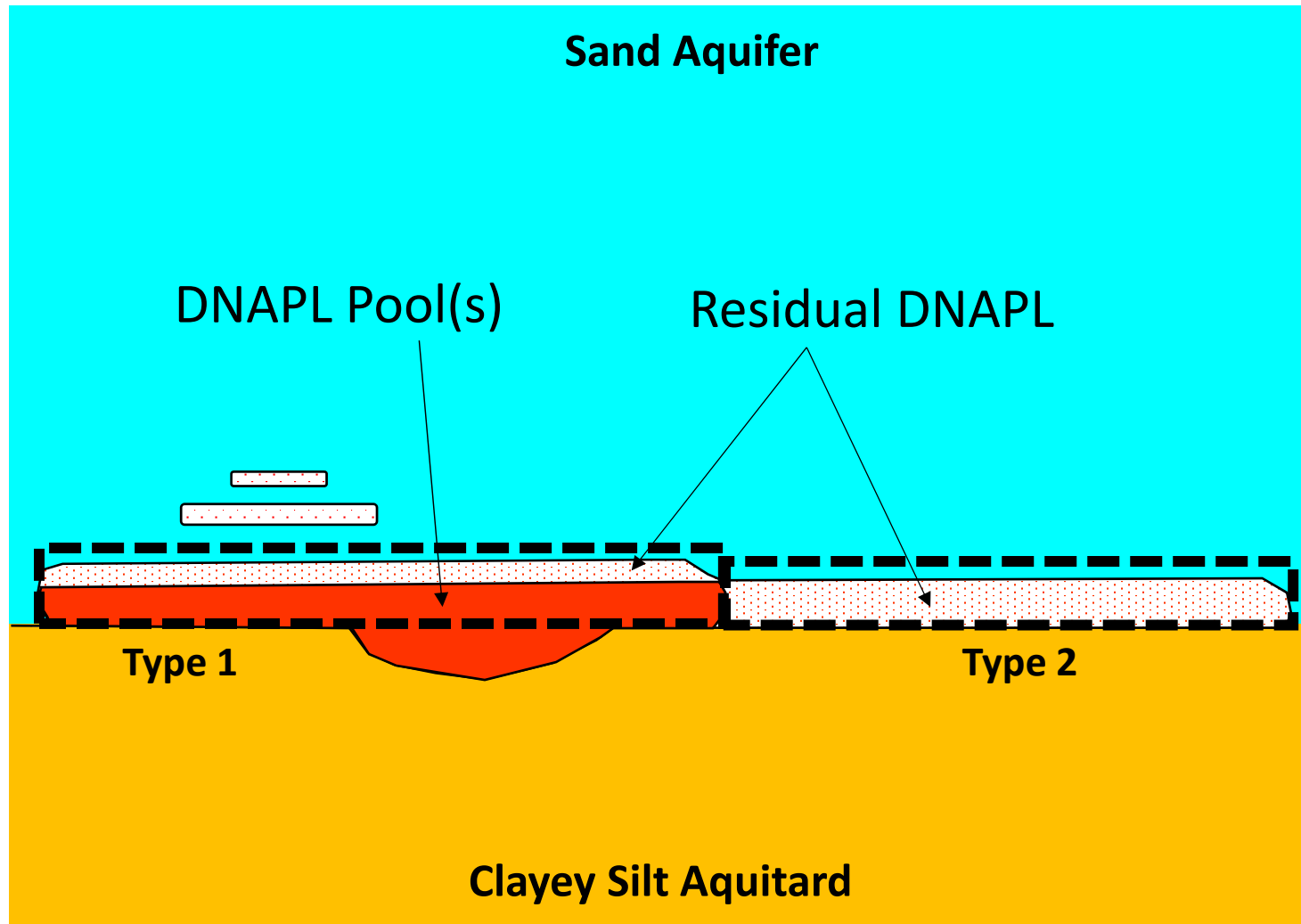
DNAPL source zone profile types:

<p><b>Type 1</b>      <math>h = \text{median thickness}</math></p> <table border="0" style="width: 100%;"> <tr> <td style="text-align: center;"></td> <td style="padding-left: 10px;"><math>h=7.5 \text{ cm}</math></td> </tr> <tr> <td style="text-align: center;"></td> <td style="padding-left: 10px;"><math>h=5 \text{ cm}</math></td> </tr> </table>		$h=7.5 \text{ cm}$		$h=5 \text{ cm}$	<p><b>Type 2</b></p> <table border="0" style="width: 100%;"> <tr> <td style="text-align: center;"></td> <td style="padding-left: 10px;"><math>h=10 \text{ cm}</math></td> </tr> </table>		$h=10 \text{ cm}$
	$h=7.5 \text{ cm}$						
	$h=5 \text{ cm}$						
	$h=10 \text{ cm}$						

# Typical DNAPL Architecture

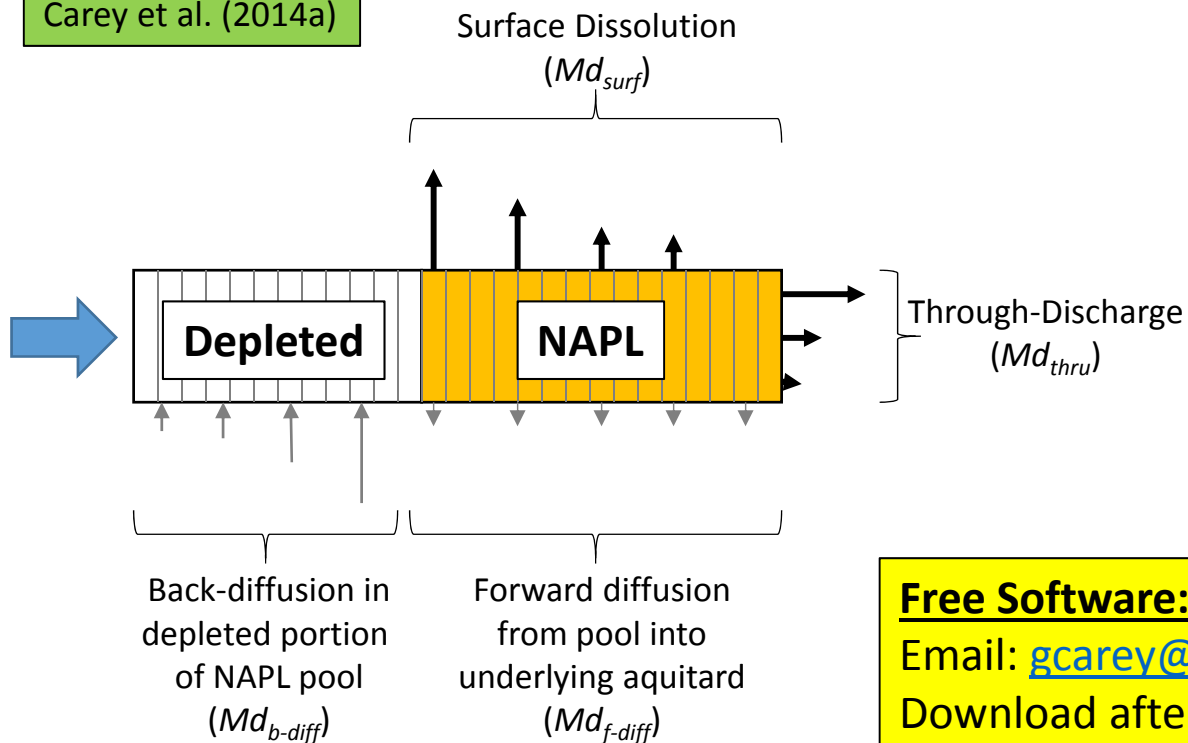


# Typical DNAPL Architecture



# NAPL Depletion Model (NDM): Mass Discharge-Based

Carey et al. (2014a)



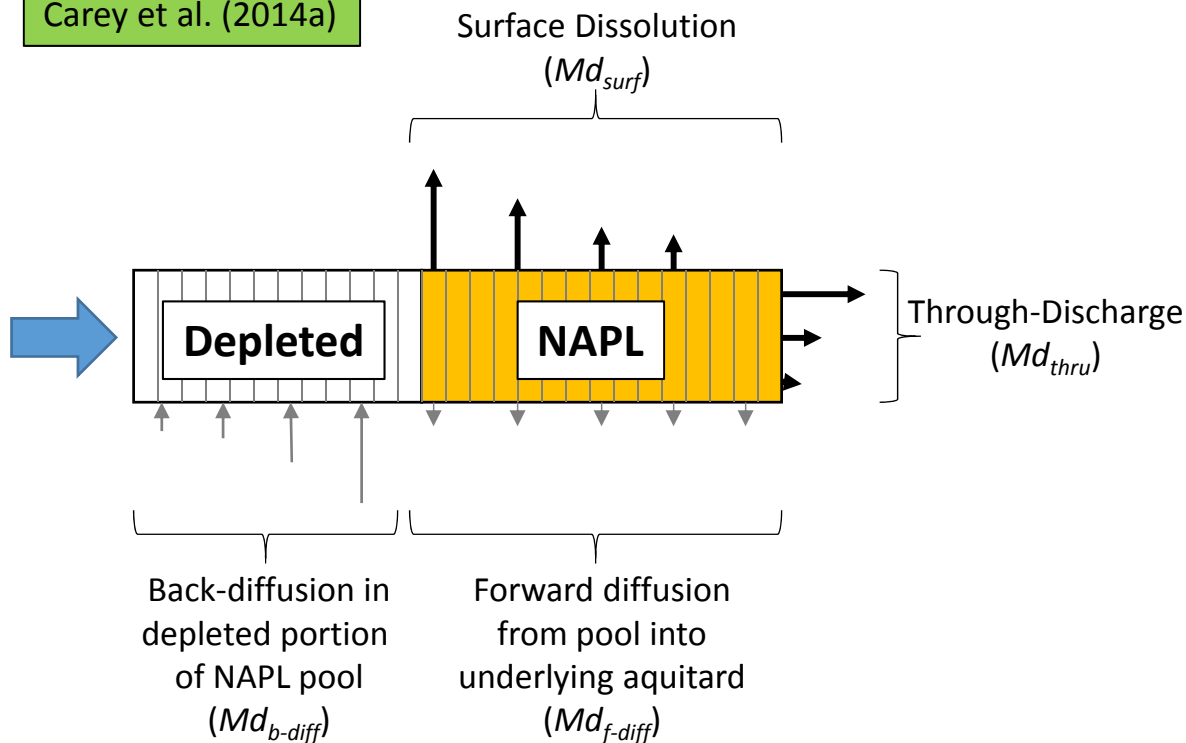
**Free Software:**

Email: [gcarey@porewater.com](mailto:gcarey@porewater.com)

Download after Sep. 30<sup>th</sup>: [www.porewater.com](http://www.porewater.com)

# NAPL Depletion Model (NDM): Mass Discharge-Based

Carey et al. (2014a)



Empirical Relationship ( $K$ in m/s)	
$\tau = 0.60 K^{0.030}$	(i)
$\theta_t = 0.30 K^{-0.026}$	(ii)
$\theta_e = 0.41 K^{0.064}, K \leq 1 \times 10^{-2} \text{ m/s}$	(iii)
$\theta_e = (0.29 K^{-0.026}) - 0.03, K > 1 \times 10^{-2} \text{ m/s}$	(iv)
$\alpha_{TV} = 0.08 K^{-0.16}, v \leq v_c$	(v)
$\alpha_{TV\_NE} = 0.08 K^{-0.16} (v_c/v)^{0.5}, v > v_c$	(vi)
$\alpha_{aw} = 0.112 (100 K)^{0.211}$	(vii)
$n = 13.14 (100 K)^{0.246}, K \geq 1 \times 10^{-4} \text{ m/s}$	(viii)
$S_{wr} = 0.015 (100 K)^{-0.218}$	(ix)

Carey et al. (2015a,b,c)

# Model Validation Goals

1. DNAPL mass in simplified source zone consistent with Chapman and Parker (2005).
2. Initial (1994) Mass discharge – estimated to be 360 to 720 kg/y.
3. Mass discharge decline half-life – estimated to be about 10 years (Chapman and Parker, 2005).

# NDM Simulation Results

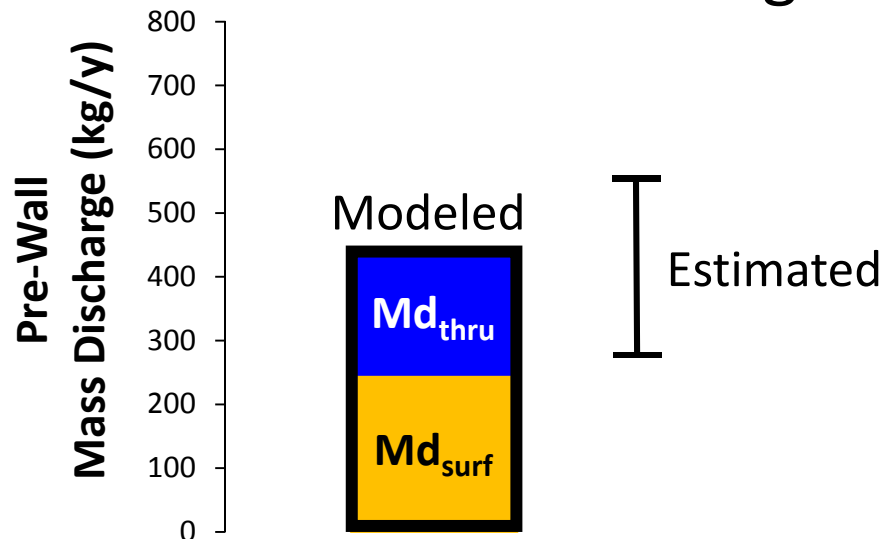
- Simulated DNAPL mass = 4,250 kg
  - Chapman and Parker (2005) estimated 5,000 to 20,000 kg
  - Our simplified source zone ignored several large areas with thicker DNAPL
    - Limited contribution to overall mass discharge
    - Simulated DNAPL mass consistent with observed on that basis



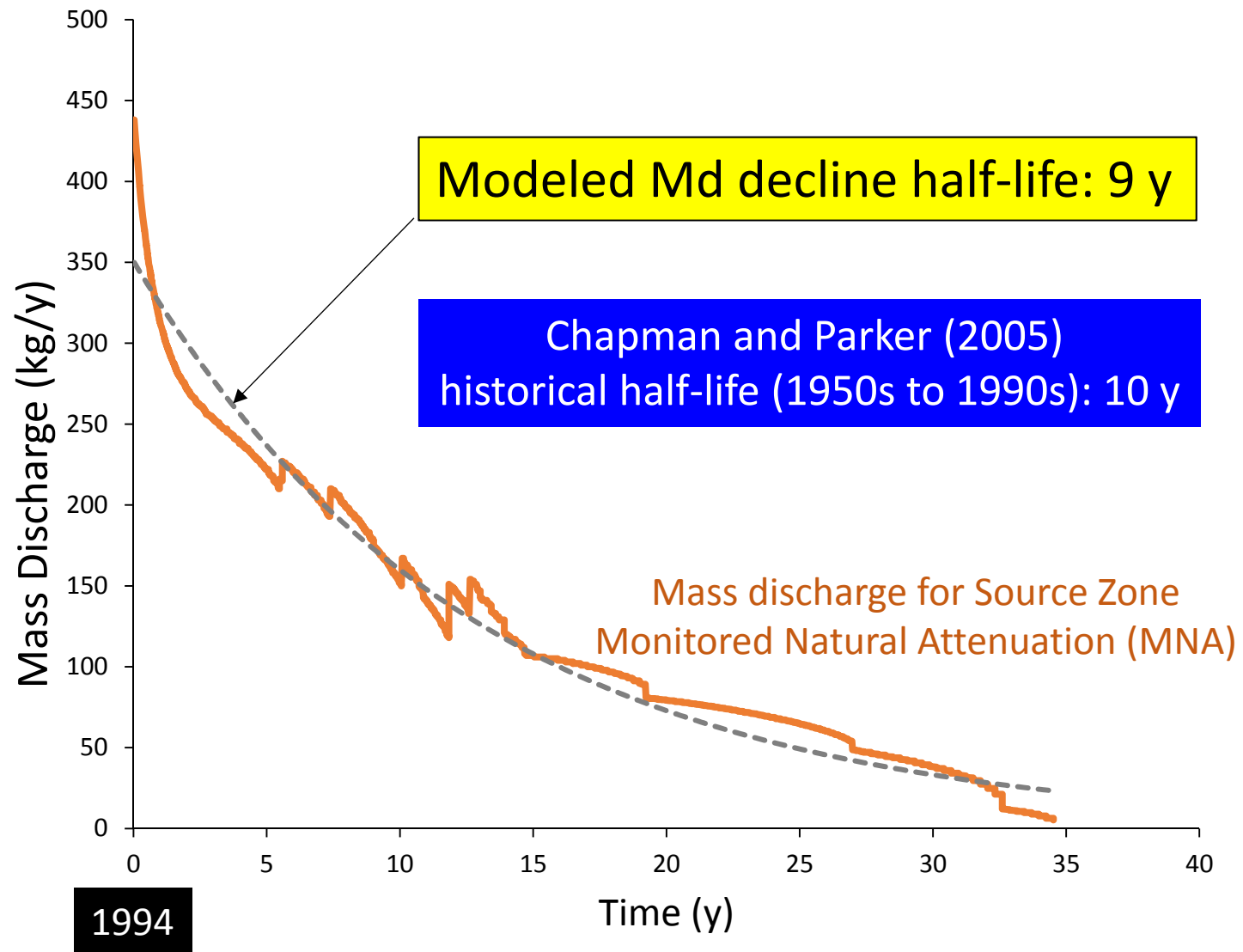
# NDM Simulation Results

- Simulated DNAPL mass = 4,250 kg
  - Chapman and Parker (2005) estimated 5,000 to 20,000 kg
  - Our simplified source zone ignored several large areas with thicker DNAPL
    - Limited contribution to overall mass discharge
    - Simulated DNAPL mass consistent with observed on that basis

- Simulated 1994 Mass Discharge



# Modeled vs. Estimated Md Half-Life



*Md = Mass discharge*

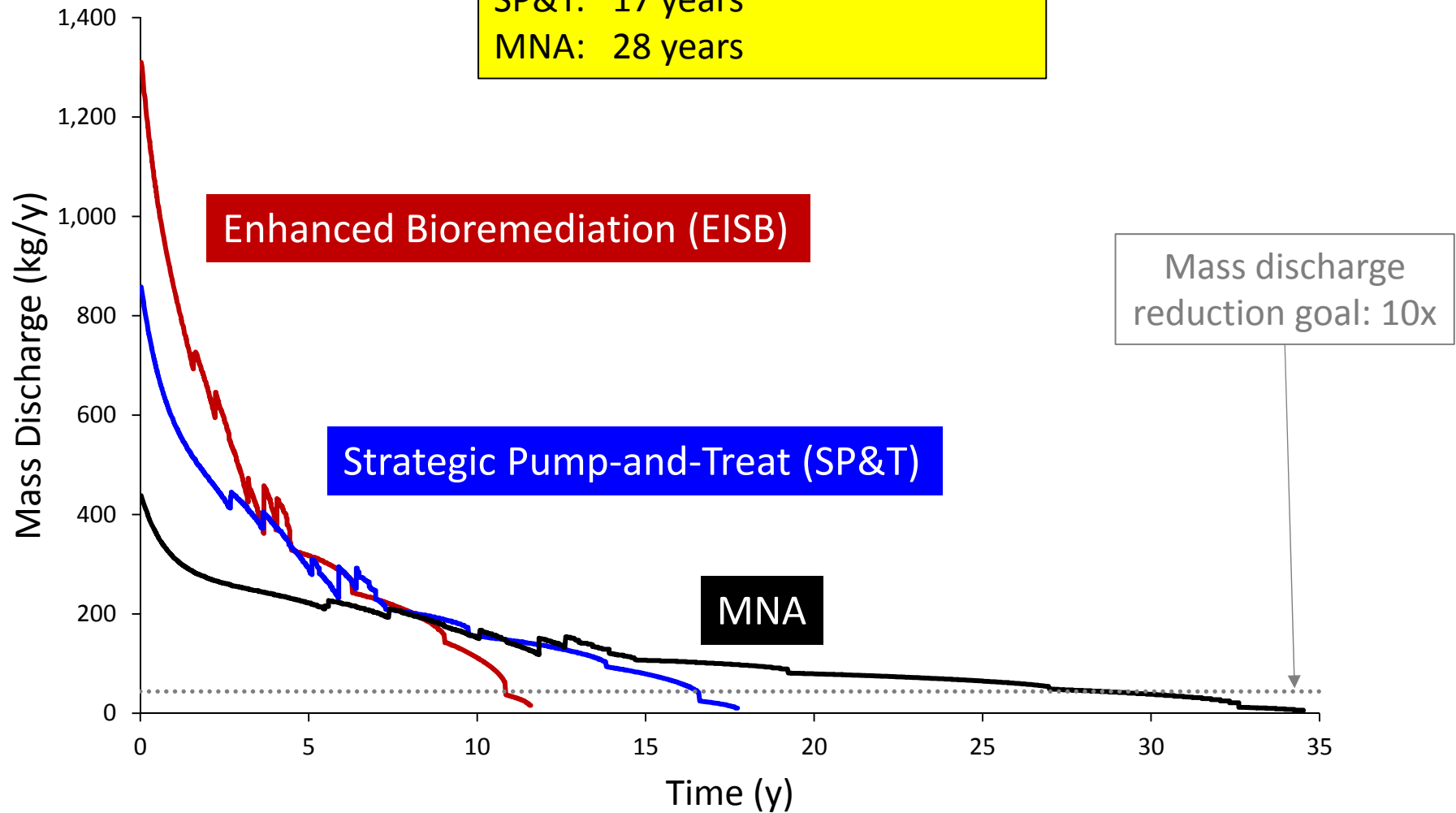
# Relative Depletion Timeframes

## Time to attain Md reduction goal

EISB: 11 years

SP&T: 17 years

MNA: 28 years



# DNAPL Architecture Sensitivity Analysis

- Varied NAPL architecture and re-ran model – any other scenarios that match **1994 Md** and **half-life?**
  - Length / 2
  - Width / 2
  - Uniform thickness of 4", 8", or 1 ft
    - a) All pooled DNAPL; or
    - b) All residual DNAPL
  - Zero flux through all DNAPL sub-zones
  - Type 1 – residual zone is suspended above pool.
- No other scenarios matched **both** observations.
  - Half-life criteria: 10 years +/- 25%

# Summary

1. We can use process-oriented NAPL depletion models when architecture well defined
  - Predict relative timeframes for natural and enhanced dissolution
  - Interpretive tool – improve our understanding
2. When architecture has higher uncertainty but still relatively well understood – may be able to use model as forensic tool
  - Evaluate range of potential architectures
  - Identify data gaps
3. Multiple goals needed to calibrate a NAPL depletion model

# Supplemental Slides

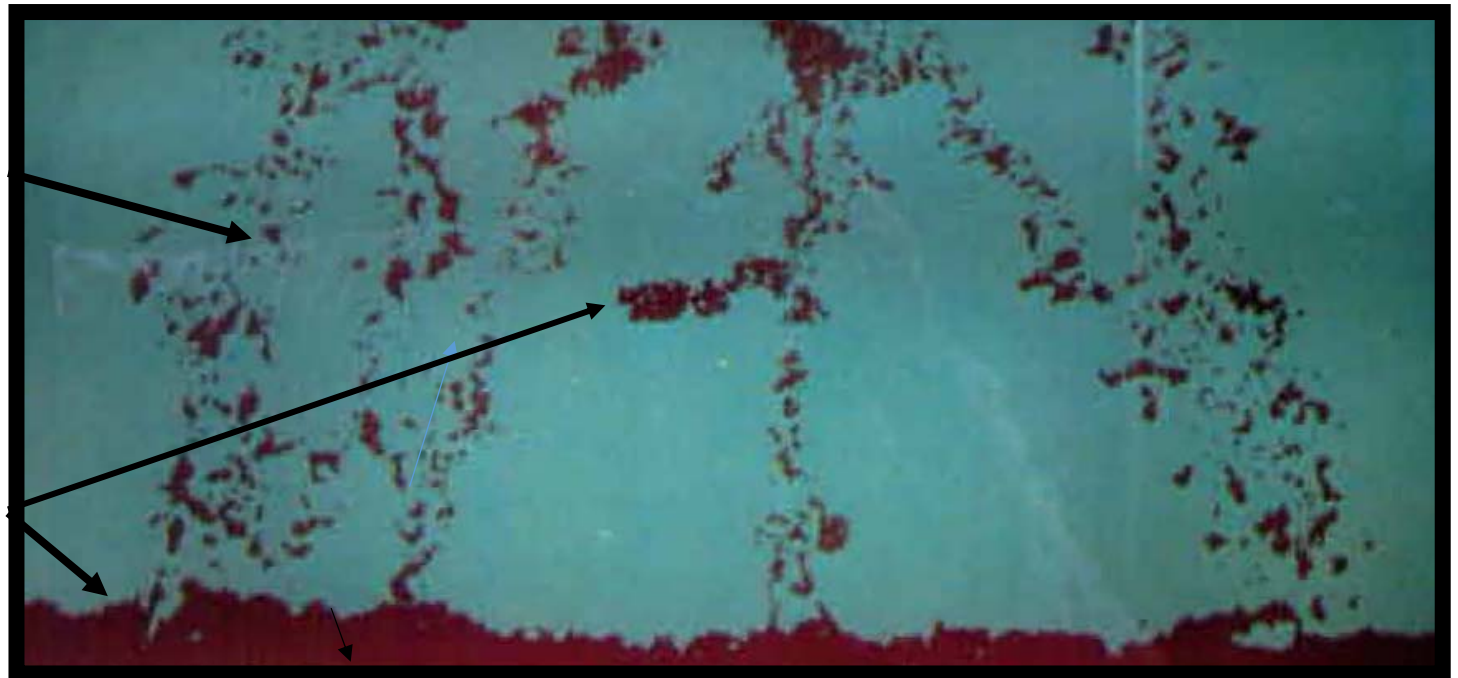
# Fresh DNAPL Source Zone

**Ganglia  
(residual NAPL)**

Timeframe: Years

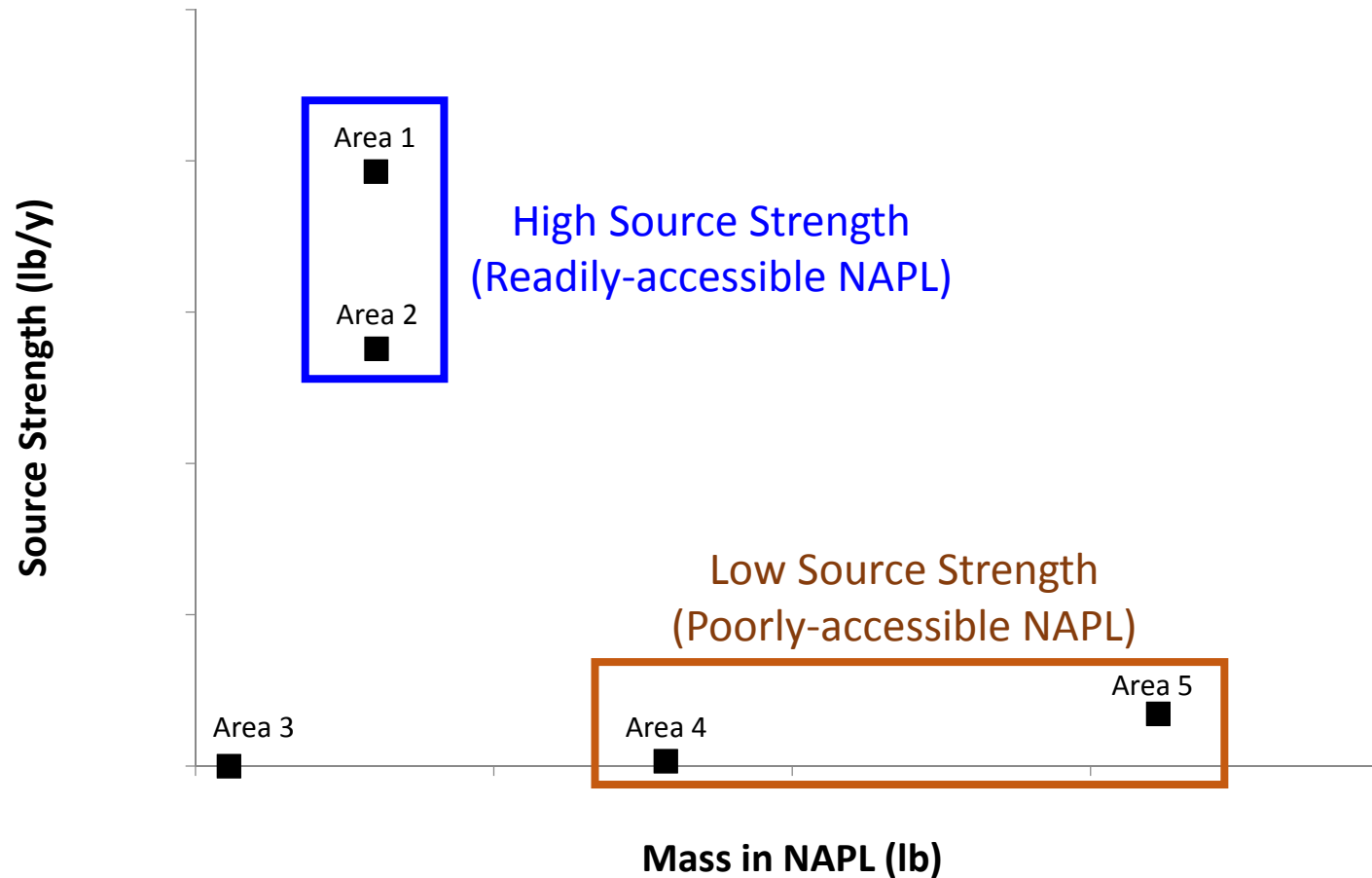
**Pools  
(free phase  
NAPL)**

Timeframe: Decades +



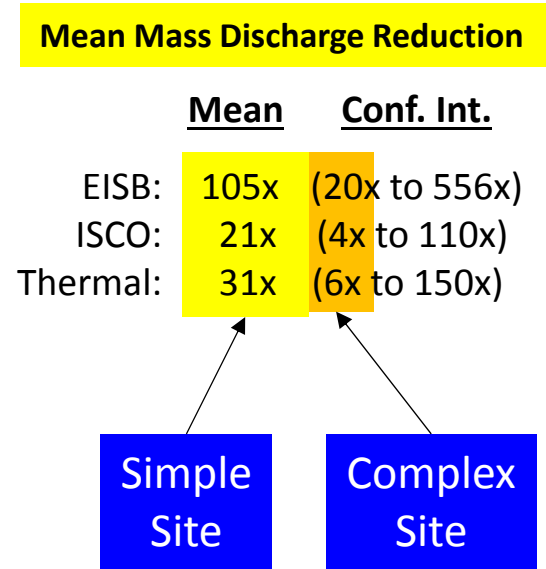
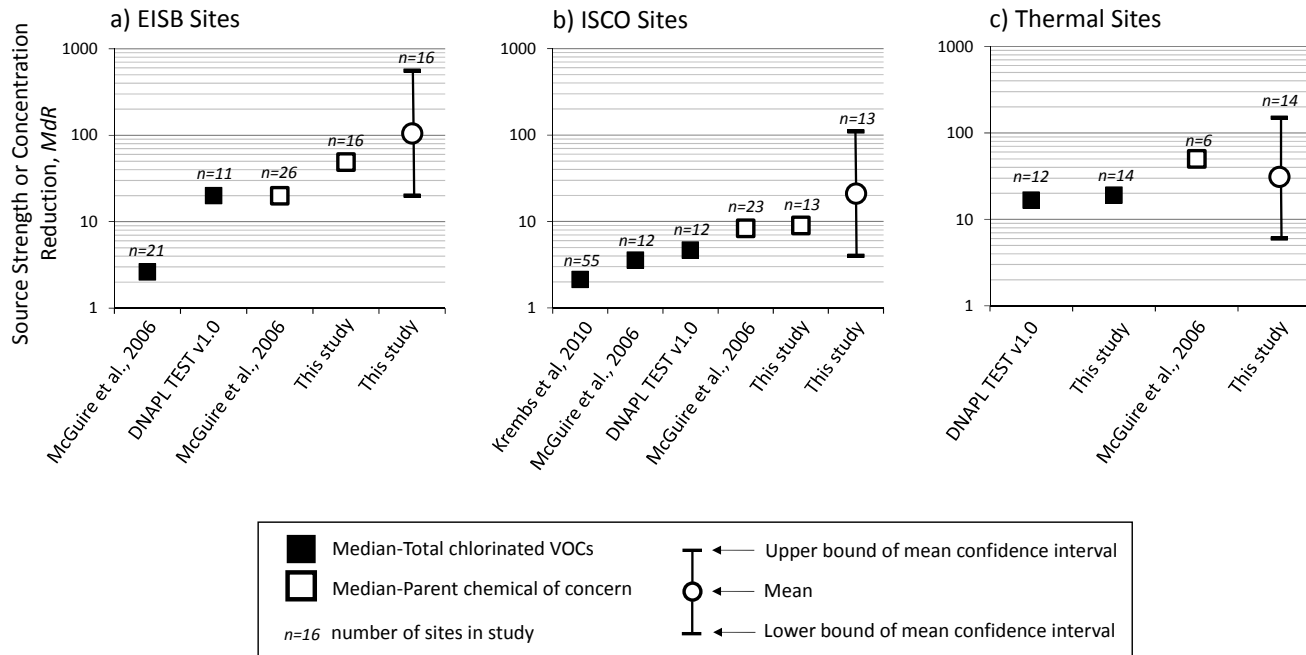
Source: Schwille, 1988

# Prioritizing Treatment Based on Mass Discharge





# Q: What is ATTAINABLE Source Strength Reduction?



Grant R. Carey

Source: Carey et al., 2014

REMEDATION Autumn 2014

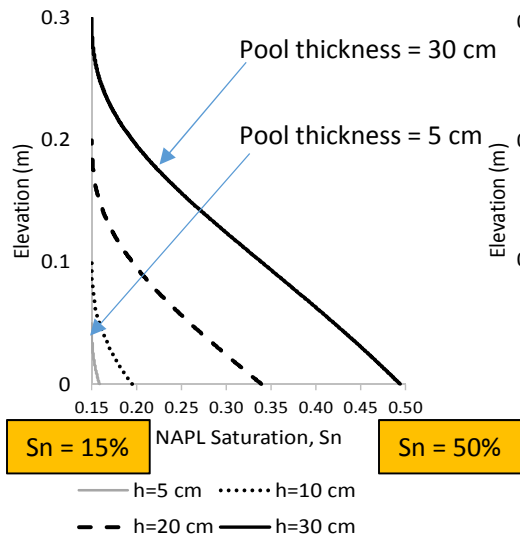
Edward A. McBean

## DNAPL Source Depletion: 2. Attainable Goals and Cost-Benefit Analyses

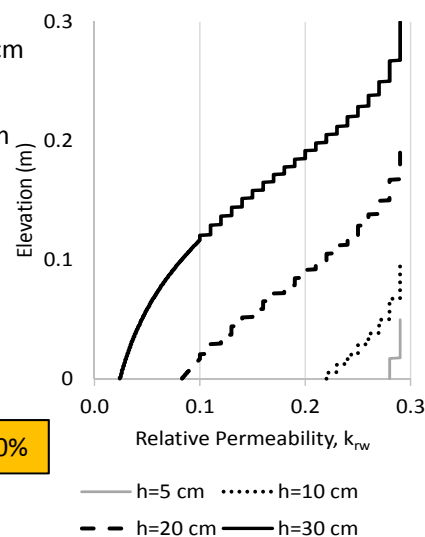
Stan Feenstra

# NAPL Saturation vs. Depth in a DNAPL Pool ( $K_{sat} = 10^{-2}$ cm/s)

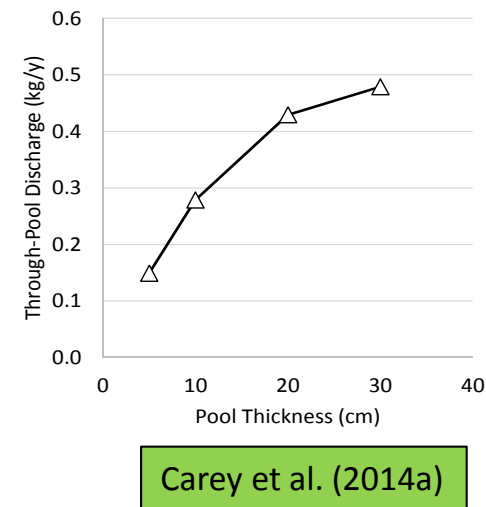
a) Elevation vs. NAPL saturation



b) Elevation vs. relative permeability

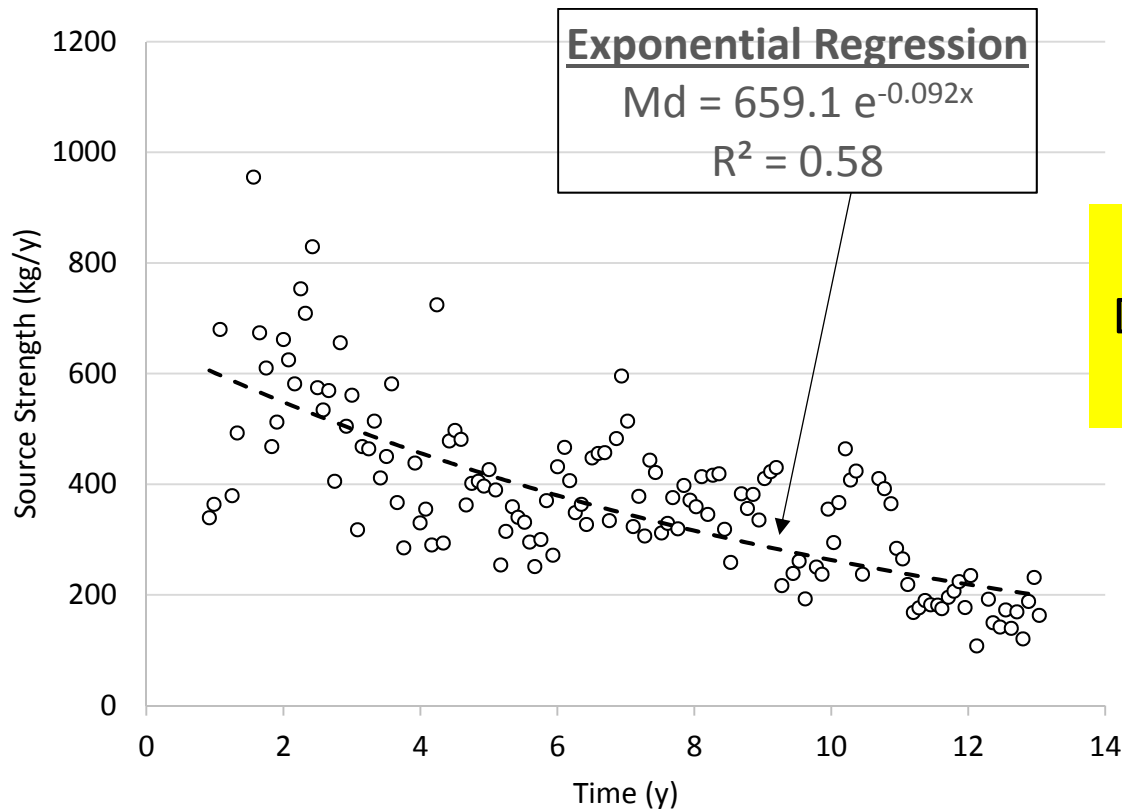


c) Through-pool discharge vs. pool thickness



Vertical distribution of DNAPL in pool – above calculations based on Eq. 3.18 in McWhorter and Kueper (1996), and assume  $P_c=0$  at the top of the pool.

# Estimating Mass: Mass Discharge Method



Initial  $Md$  ( $Md_0$ ) = 660 kg/y  
Decline rate ( $\lambda_{Md}$ ) = 0.092  $y^{-1}$   
Decline half-life = 7.5 y

Graph modified from Brusseau et al. (2011)

# Estimating Mass: Mass Discharge Method

Estimating initial mass ( $M_o$ ) in source zone (based on Newell et al., 2005):

$$M_o = Md_o / \lambda_{Md} \quad [M_o \text{ in kilograms, } Md_o \text{ in kg/y, and } \lambda_{Md} \text{ in } y^{-1}.]$$

Example calculation for Tuscon Airport Site:

$$\begin{aligned} M_o &= (660 \text{ kg/y}) / (0.092 \text{ y}^{-1}) \\ &= 7,164 \text{ kg} \sim \text{Minimum NAPL mass in subsurface} \end{aligned}$$

Calculation assumes uniform decline rate, and  
based on readily-accessible NAPL mass.

**May underestimate mass in pool-dominated source zones.**