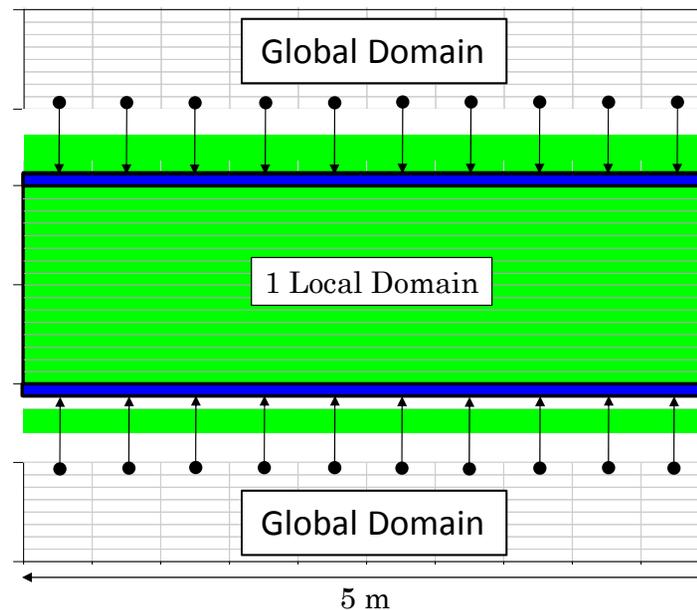
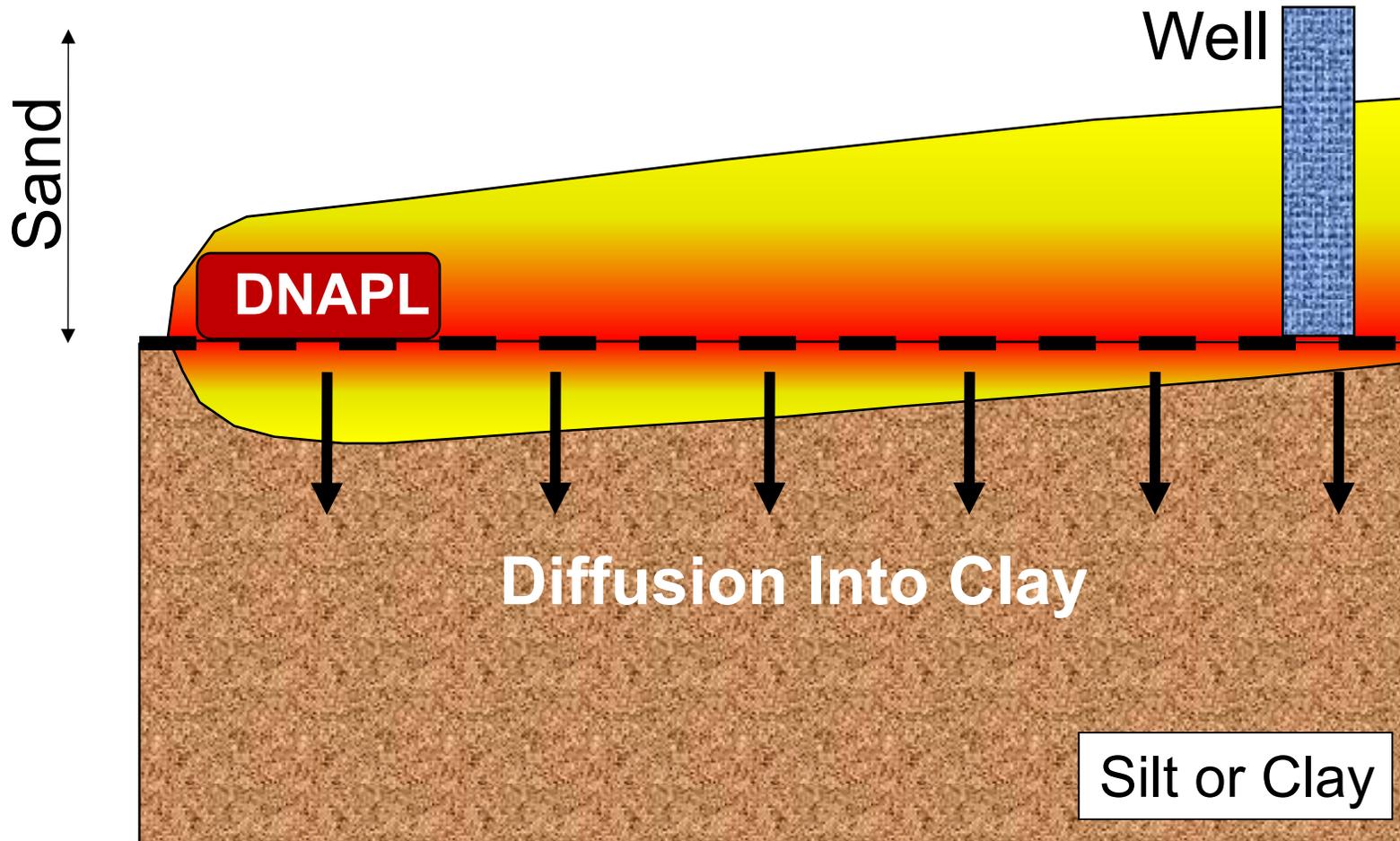


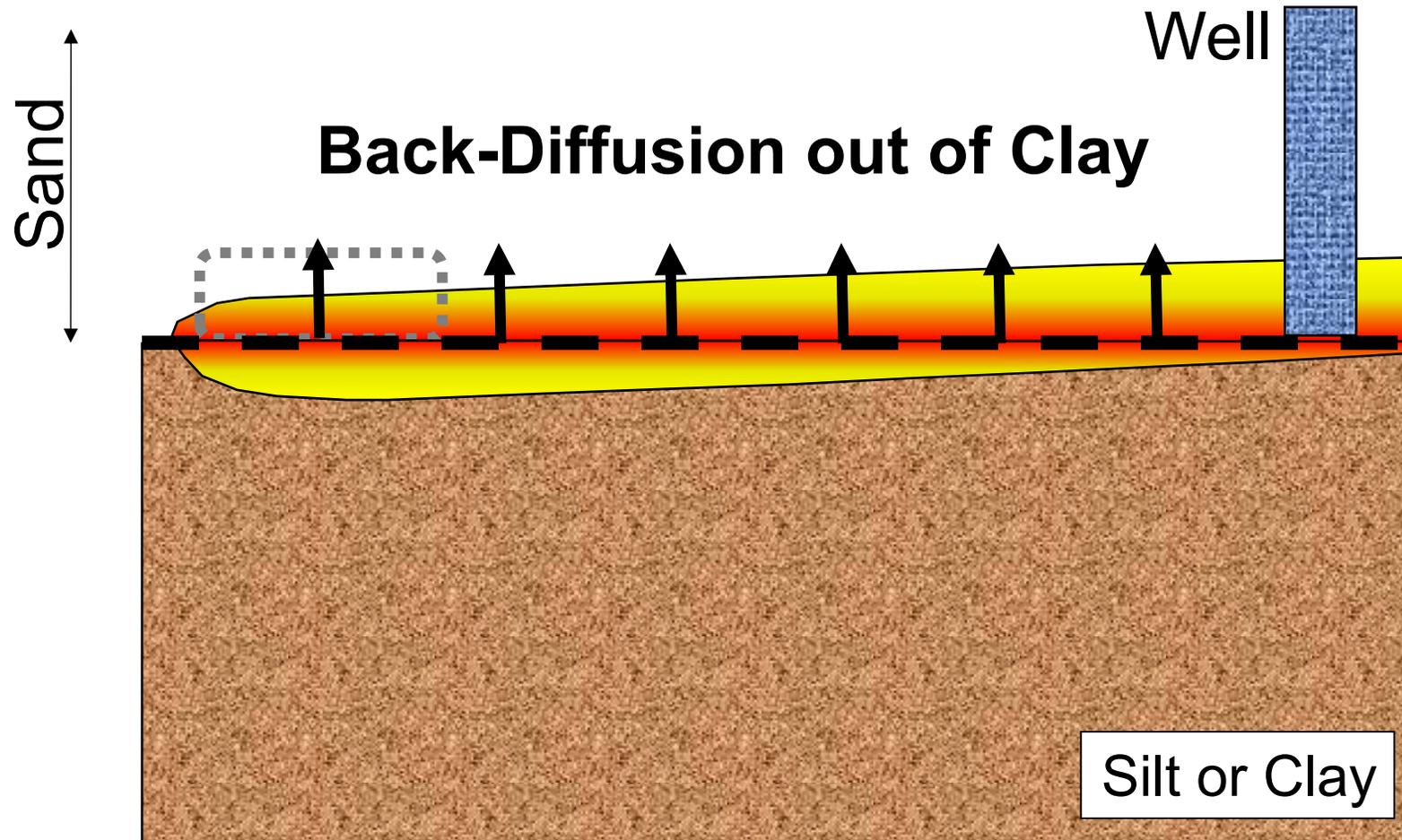
In-Situ Remediation (ISR-MT3DMS™) Local Domain Approach



Forward Diffusion



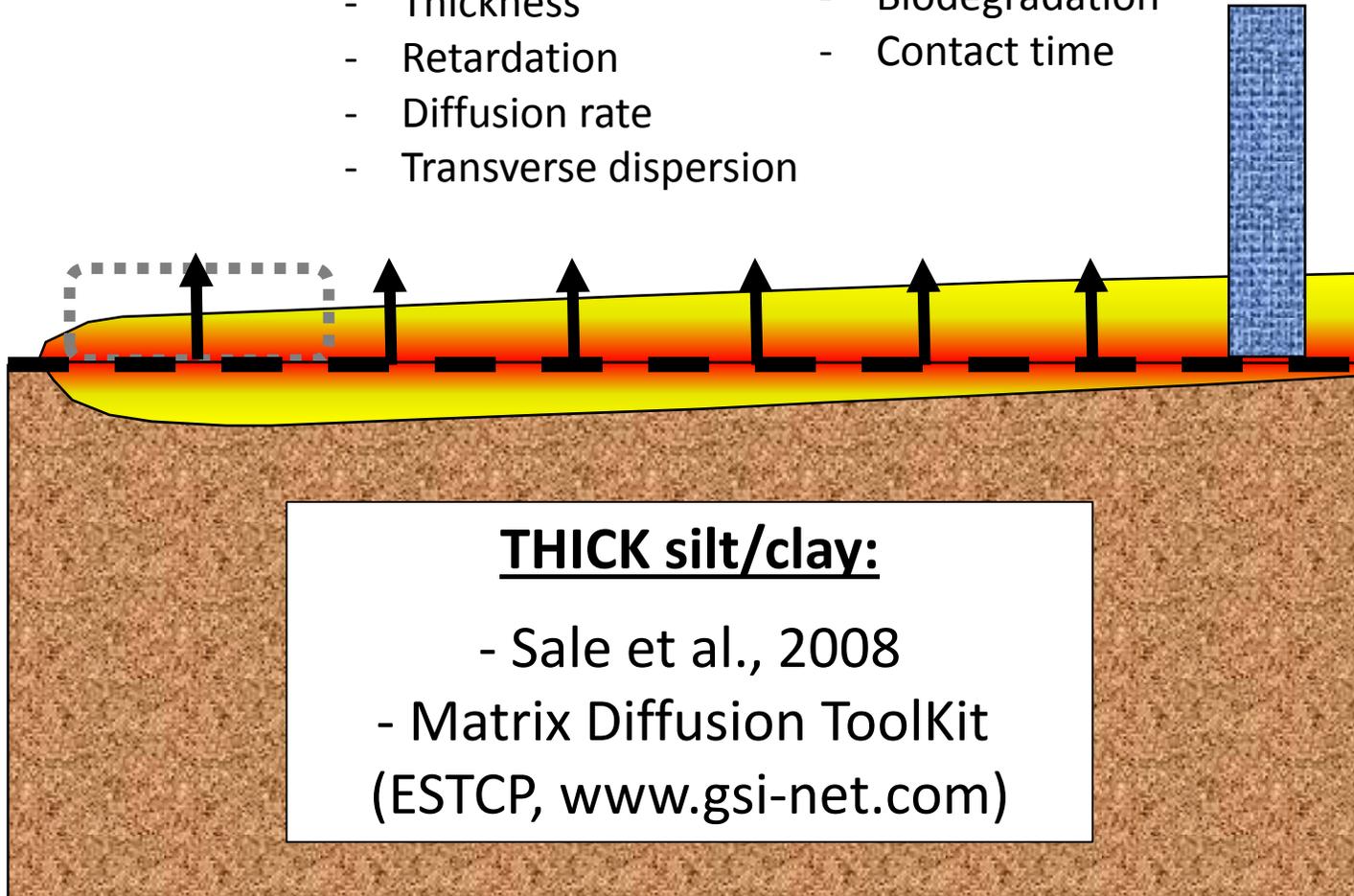
Back-Diffusion



Factors Influencing Remediation Timeframe

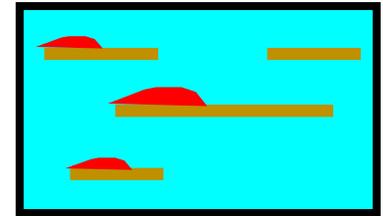
Influencing factors:

- Velocity
- Thickness
- Retardation
- Diffusion rate
- Transverse dispersion
- Length of clay lens
- Biodegradation
- Contact time



Introduction

- Modeling diffusion-dominated transport may require the addition of dozens to hundreds of layers to a model, depending on the thickness of silt/clay layers. This can have prohibitive costs, particularly for 3-D models which already incorporate a large number of rows and columns.
- While there are analytical solutions for simulating diffusion in thicker layers of silt/clay, a numerical model is often needed for thinner silt/clay layers, or when complex degradation reactions occur.

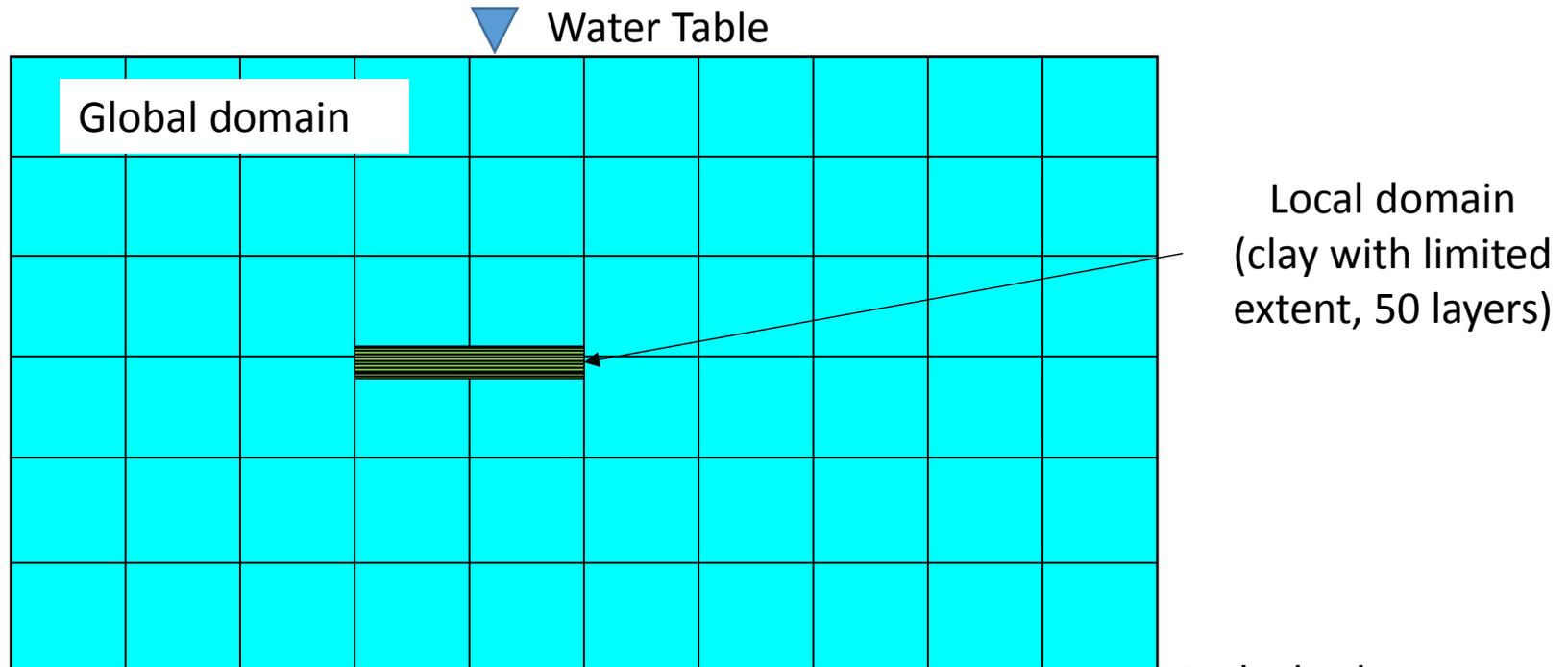


Introduction

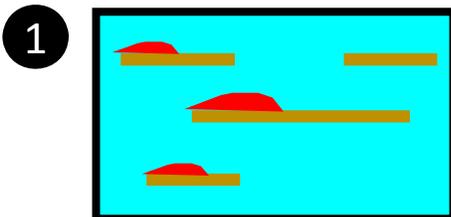
- ISR-MT3DMS™ offers the option to use local 1-D domains to represent diffusion-dominated transport. These 1-D domains are outside the global model grid, and thus may result in significant cost and time savings for some sites.
- The local 1-D domains incorporate the same reaction options that are available for the global model, so the effects of in-situ bioremediation or ISCO, for example, may be simulated in silt/clay layers.
- Users also have the option to specify different horizontal and temporal discretization for the local 1-D domains, relative to the global model.



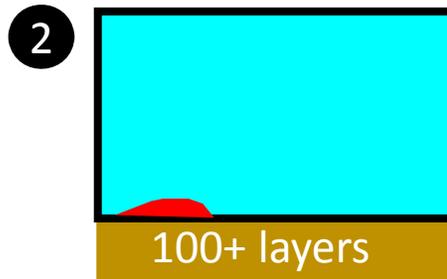
Example Applications



Each clay lens:
20 to 100+ layers

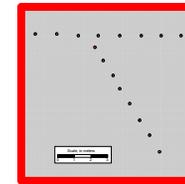
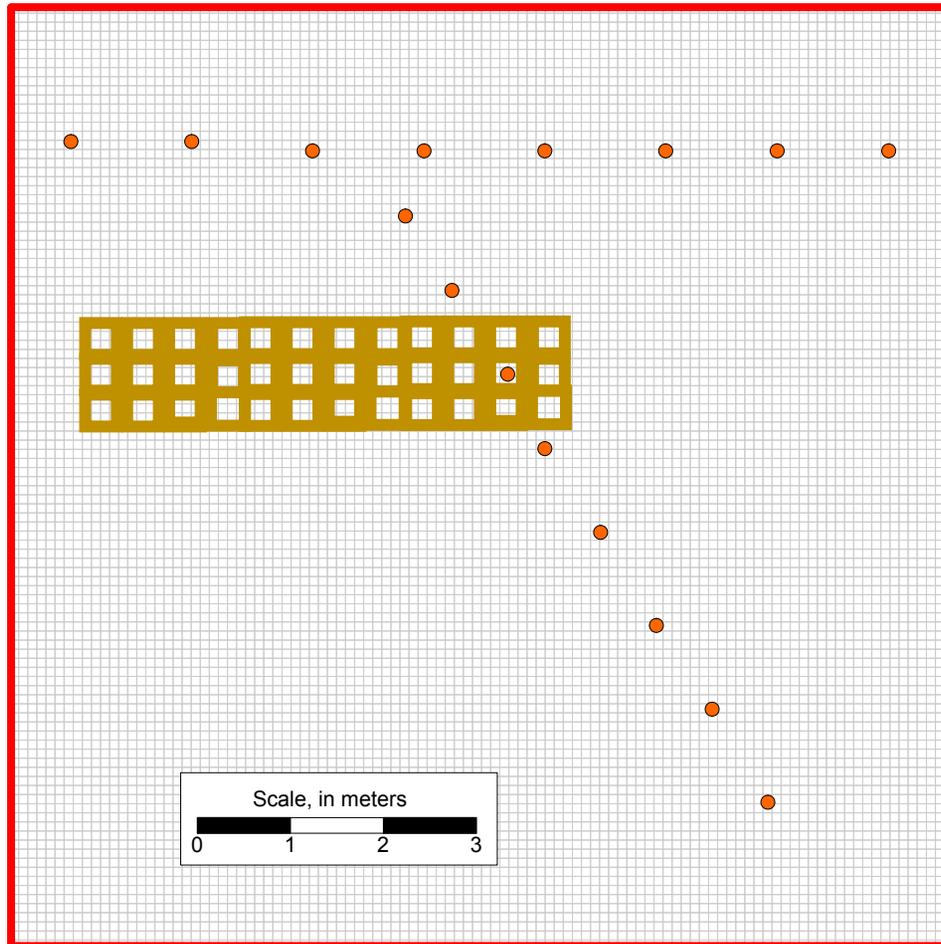


Each clay lens:
10 to 100+ layers



Expertise • Experience • Innovation

Example Applications

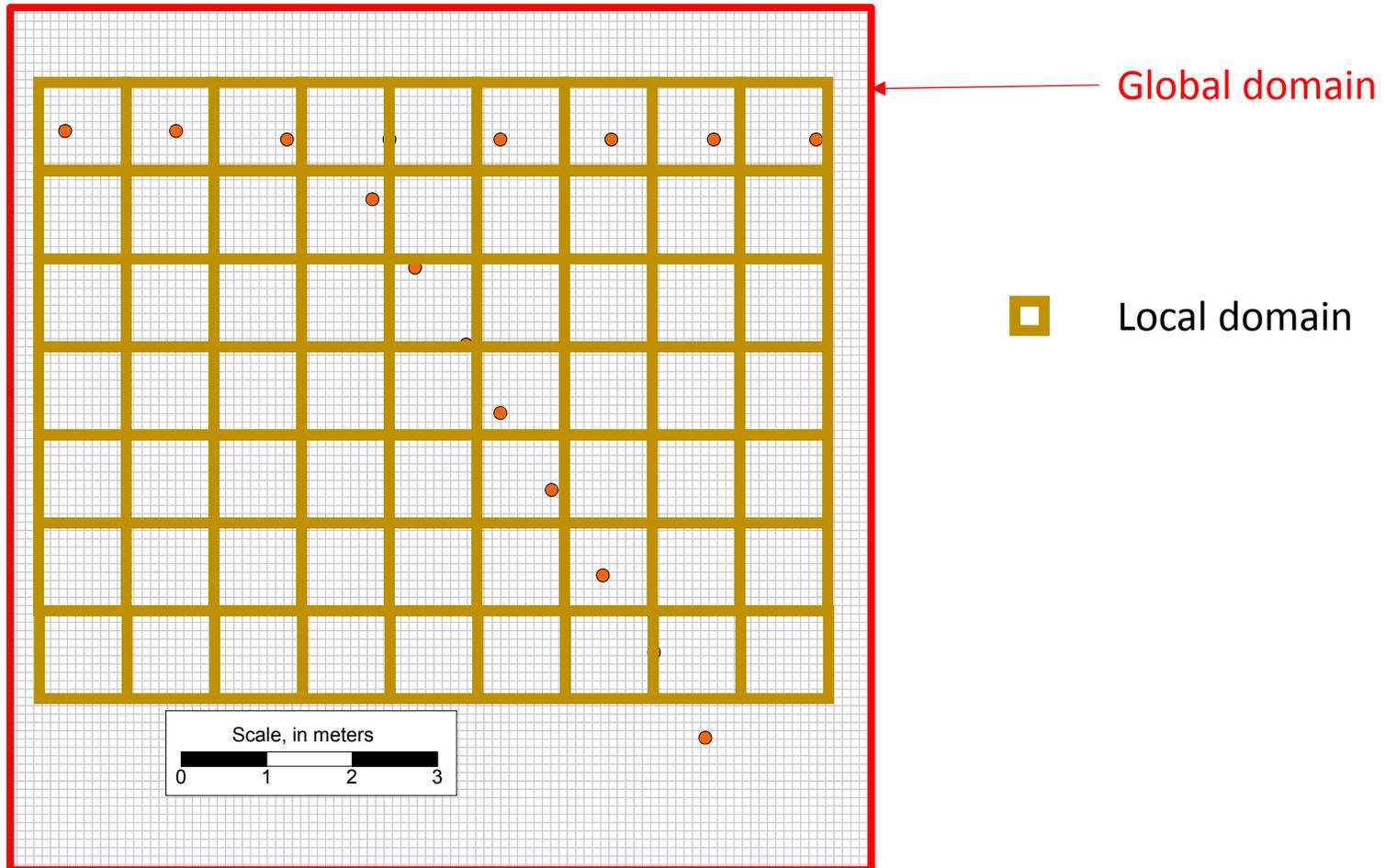


Global domain



Local domain

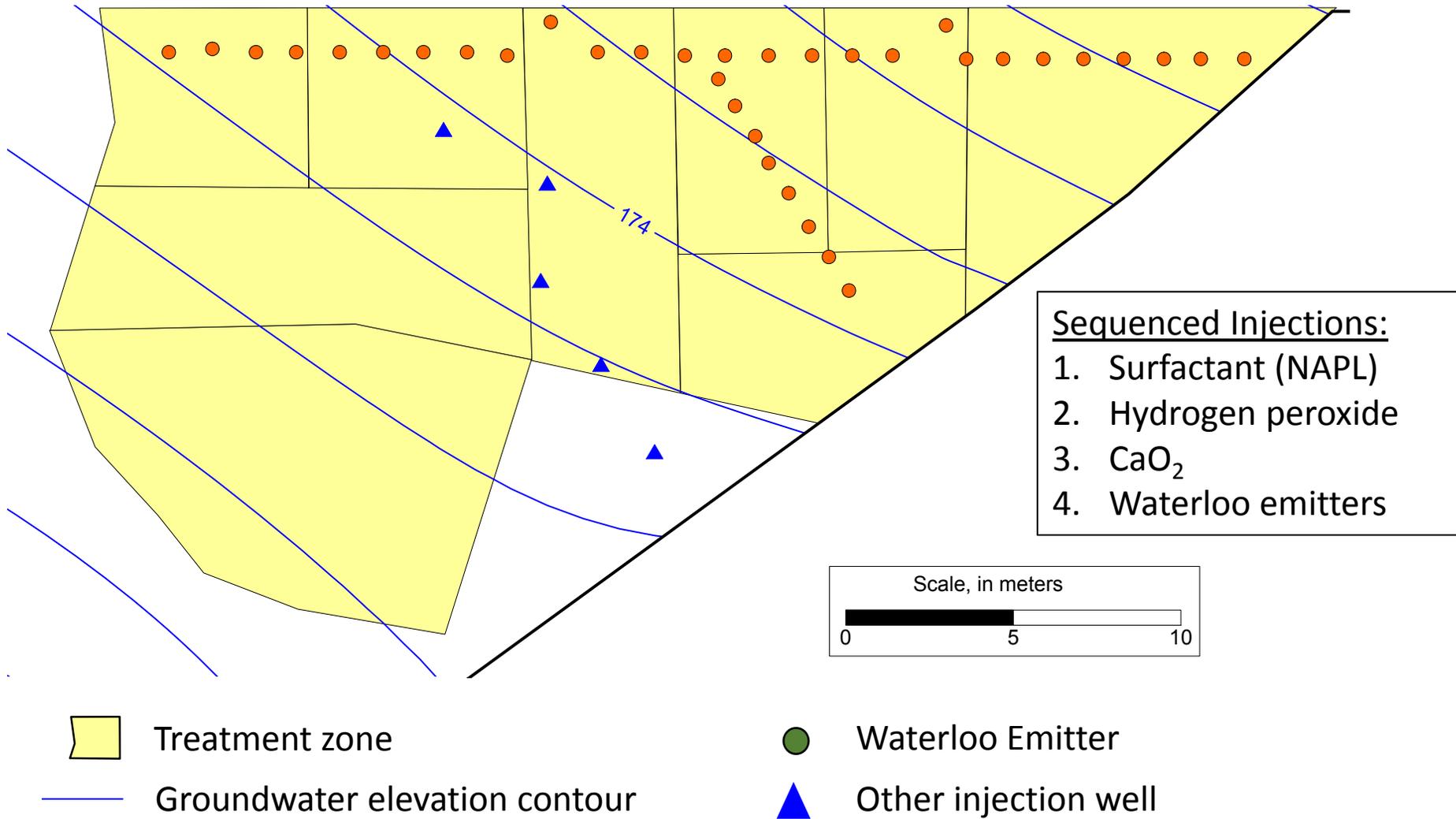
Example Applications



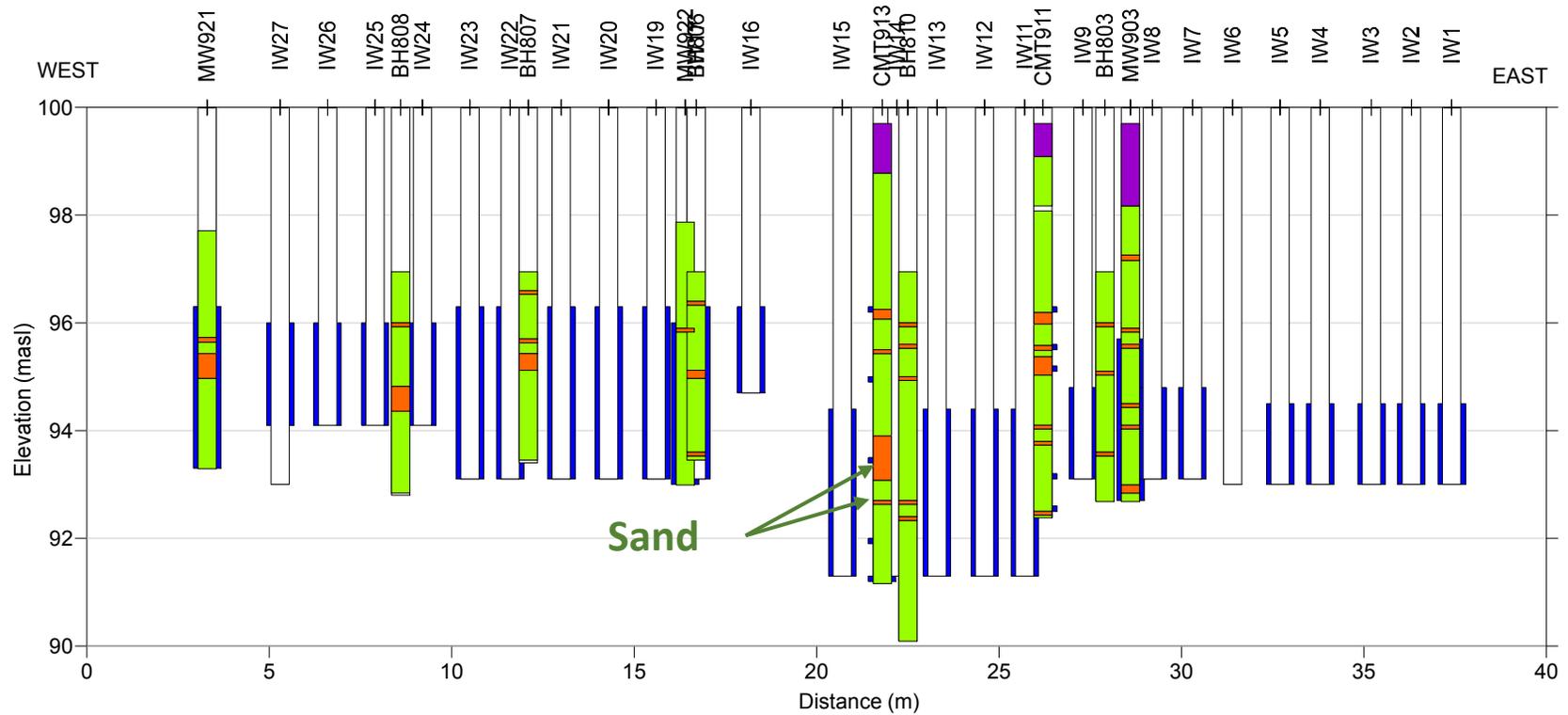
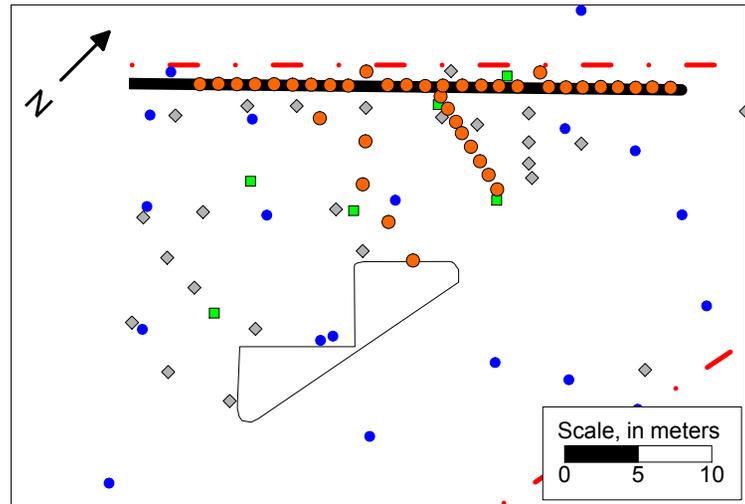
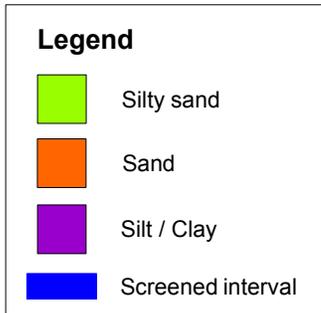
Example #1: Ontario Site



Case Study #1 – Ontario Site



Section K-K'



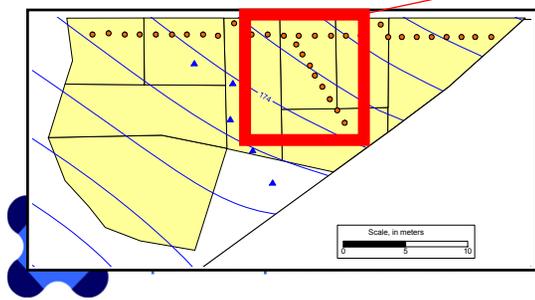
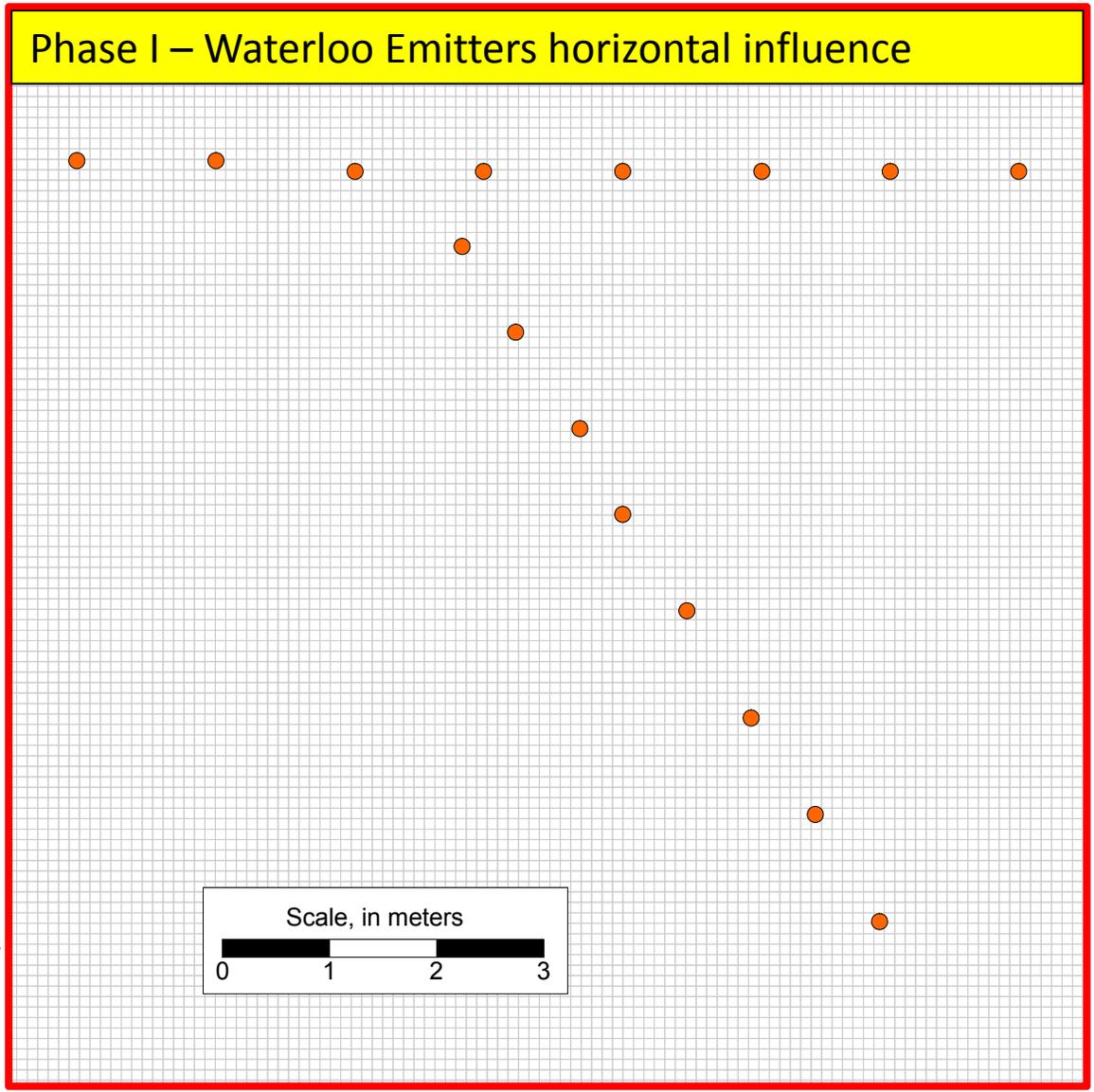
Model Grid

Minimum spacing = 4 inches
(Waterloo Emitter diameter)

2-D: 450 columns, 280 rows

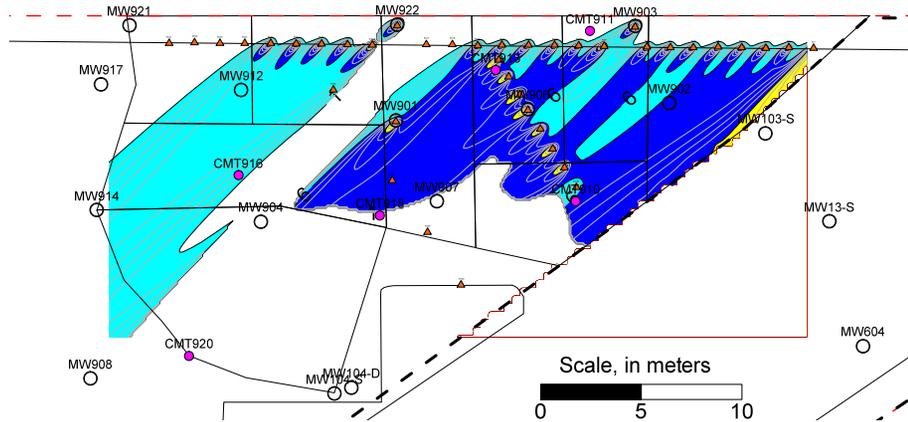
Time step = 0.05 d

Phase I – 5 solutes
(4-hour run-time)

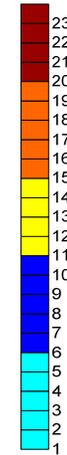


Phase I: Waterloo Emitters (t=3y)

Case 1: PHC Koc = 5,000 mL/g



DO (mg/L)



Electron Donors:

- GRO, DRO, Fe(II)

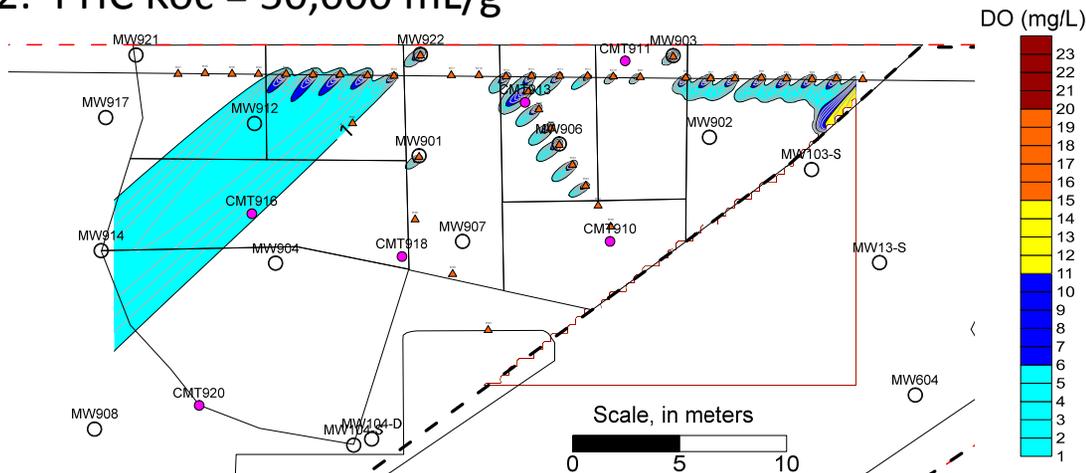
Electron Acceptors:

- DO, Fe(III)_s

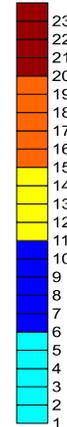
Reactions:

- Instantaneous or first-order
- Reductive dissolution

Case 2: PHC Koc = 50,000 mL/g



DO (mg/L)



Phase II model:

- Hydrogen peroxide
- CaPO
- GRO/DRO Conc.
- **Diffusion into silt**

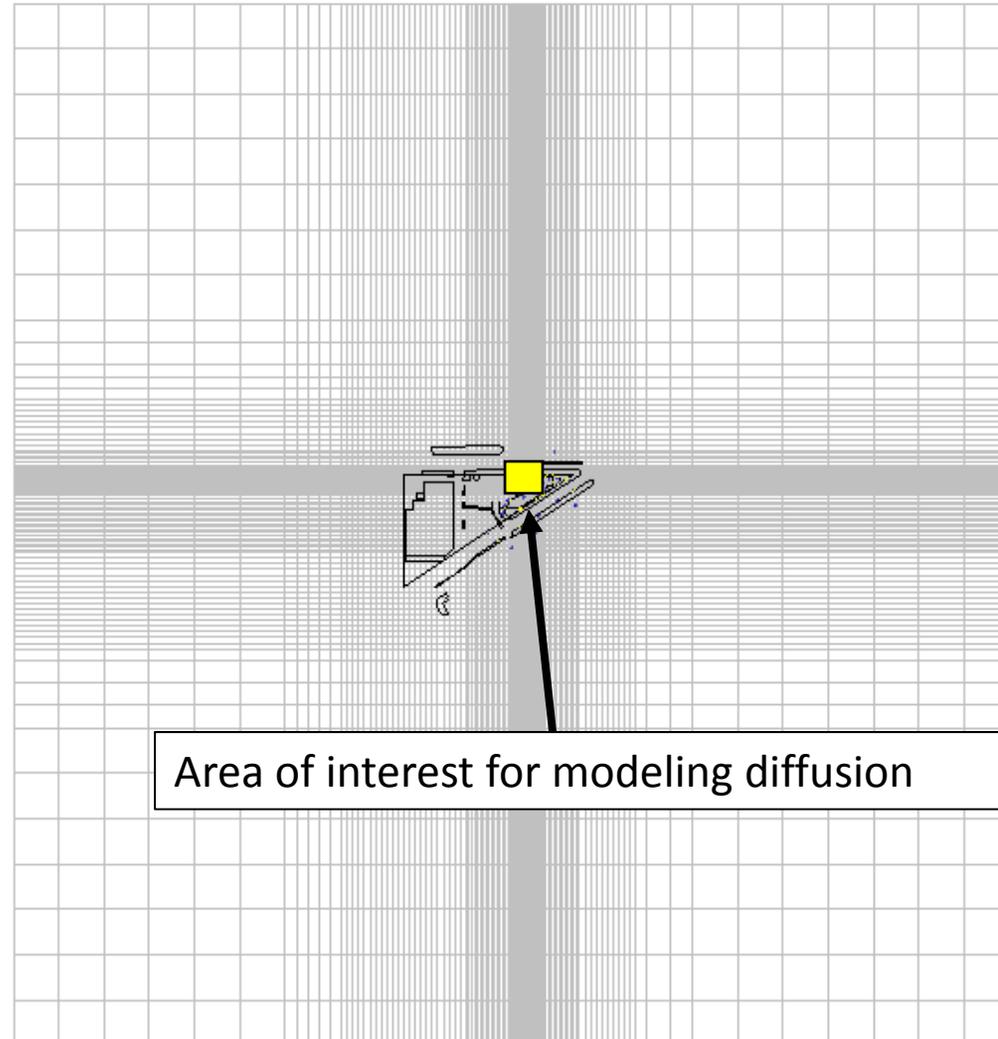
Case Study #1

- Waterloo emitters used for passive oxygen injection, with approx. 1 meter spacing between wells
- Same wells also used for periodic active injections of oxygen-releasing compound, chemical oxidant, or surfactant (depending on the event)
- Tight spacing of passive injection wells required high resolution grid discretization to evaluate zone of influence from passive injections
- Geology is interbedded sands with tight fine-grained layers.
- Costs were prohibitive to develop a 3-D model for evaluating vertical diffusion-dominated transport in thick fine-grained layers, given tight horizontal spacing and number of species in reactive transport model.

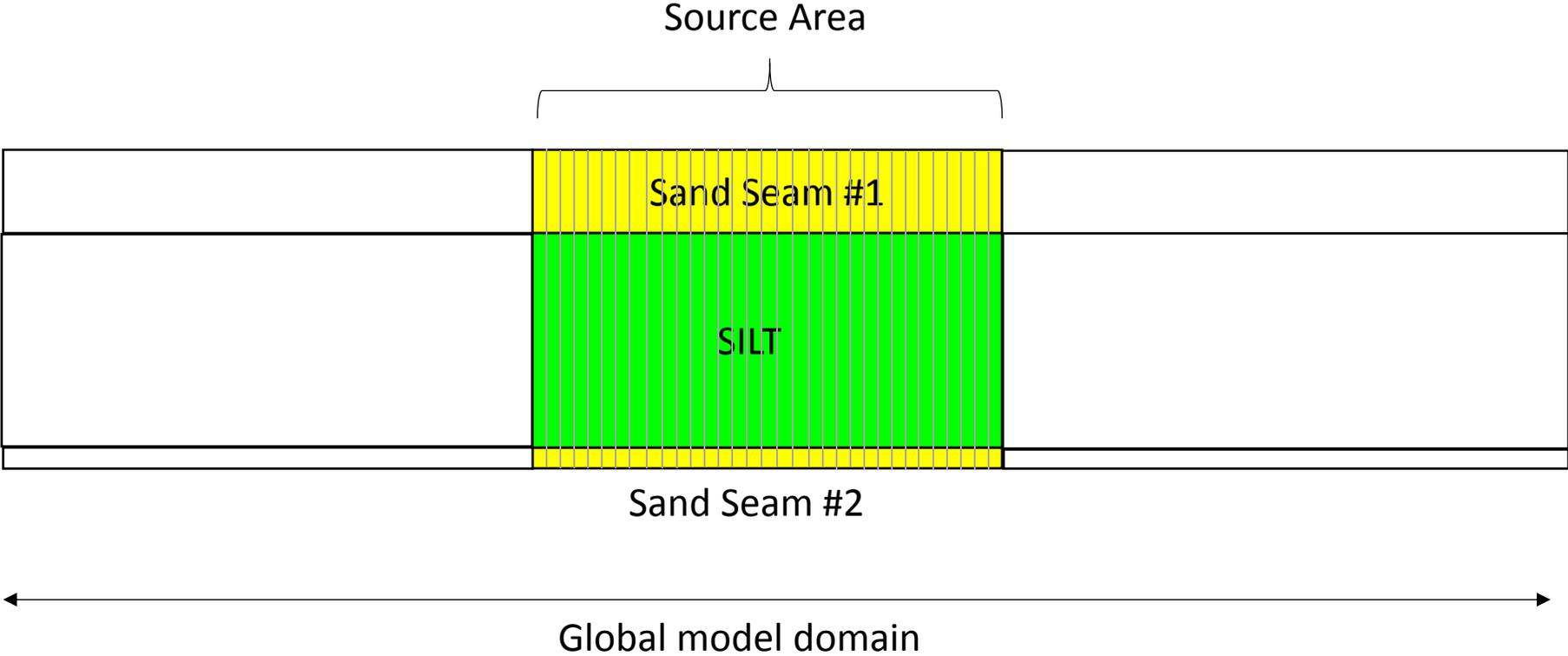


Local Domain Approach

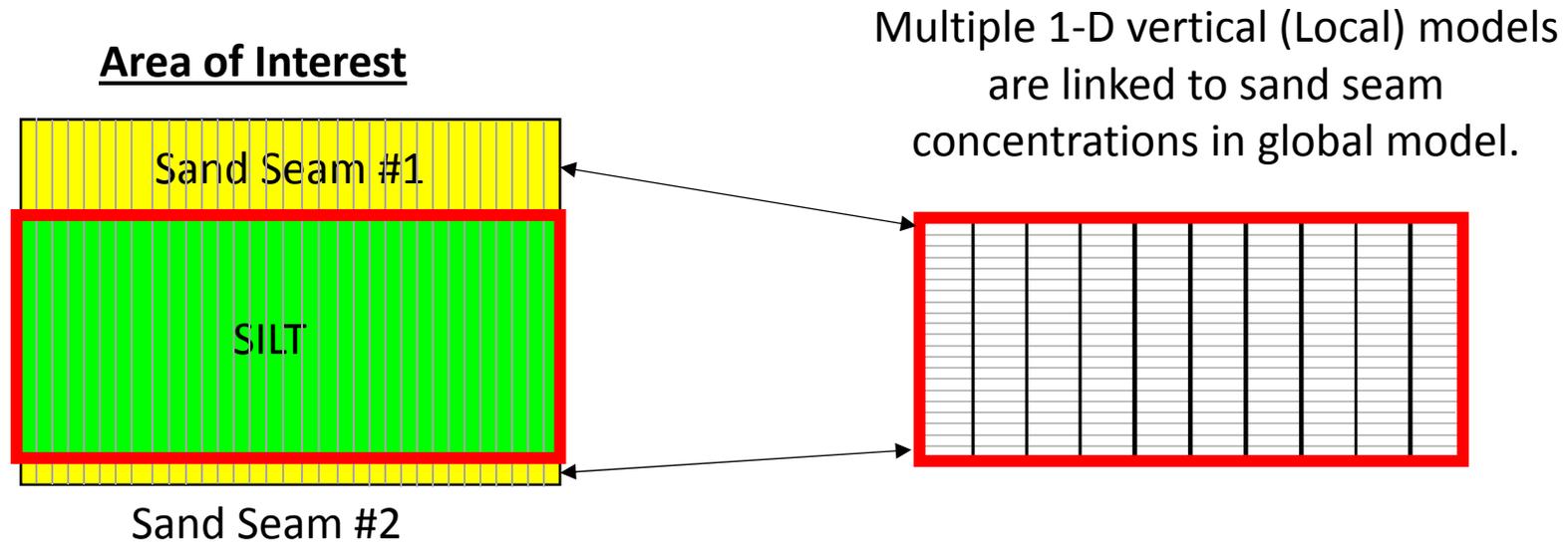
Global Model Domain



Cross-Section in Global Model (3 layers)



Local Model Domains for Silt (1-D Diffusion)



Silt layer is inactive to transport in global model.



Next Steps

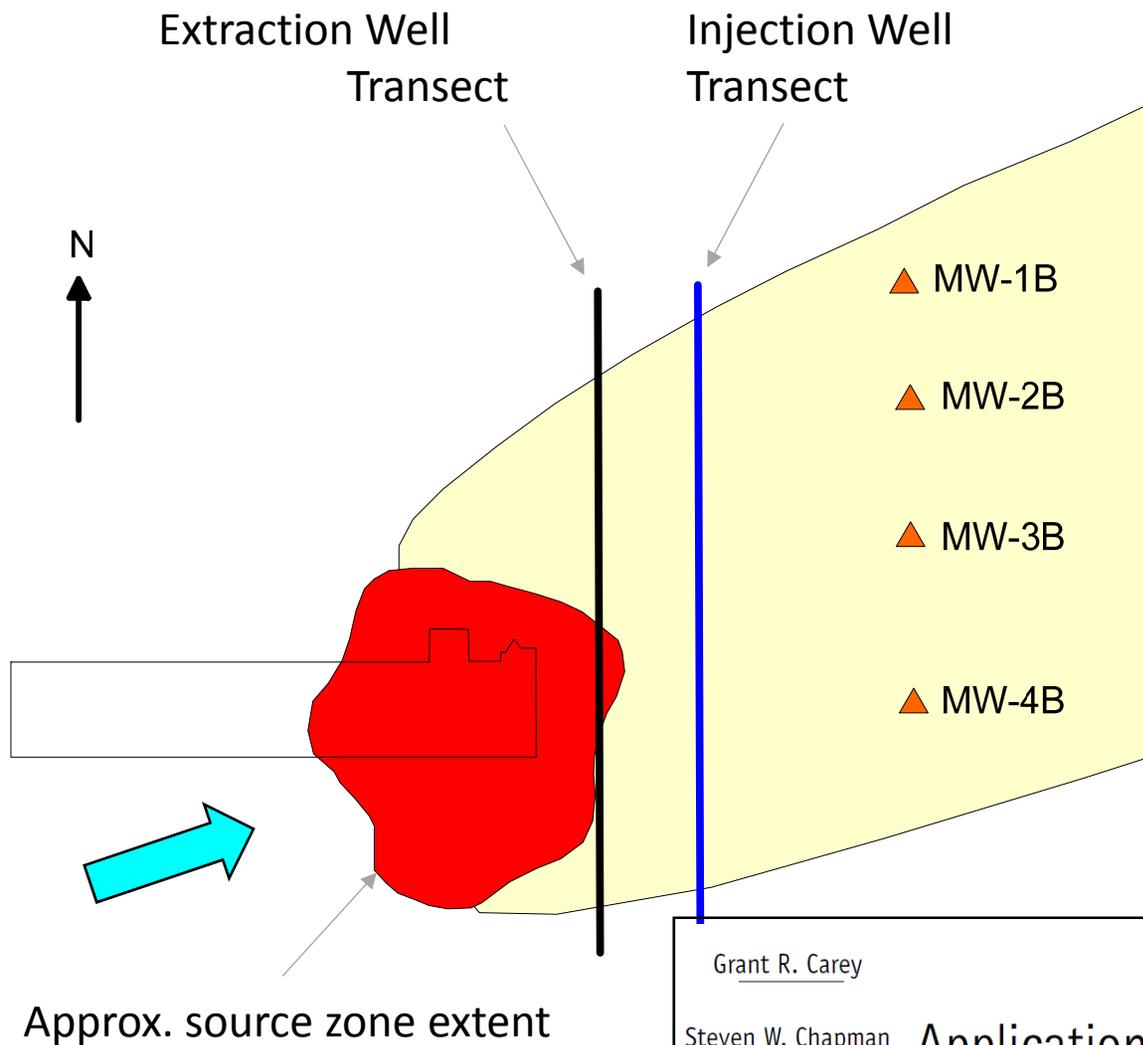
- Using the local domain approach substantially reduced the size of the global model domain.
- We are currently simulating the influence of active remediation on mass in the finer-grained layers using the local domain approach.



Case Study #2: Florida Site



Case Study – Florida Site



Site Characteristics

- Beach sand aquifer
- Continuous, thin clay layer across site
- Other discontinuous, thin silt/clay layers
- Multiple, thin suspended DNAPL layers in source zone

Grant R. Carey

Steven W. Chapman

Beth L. Parker

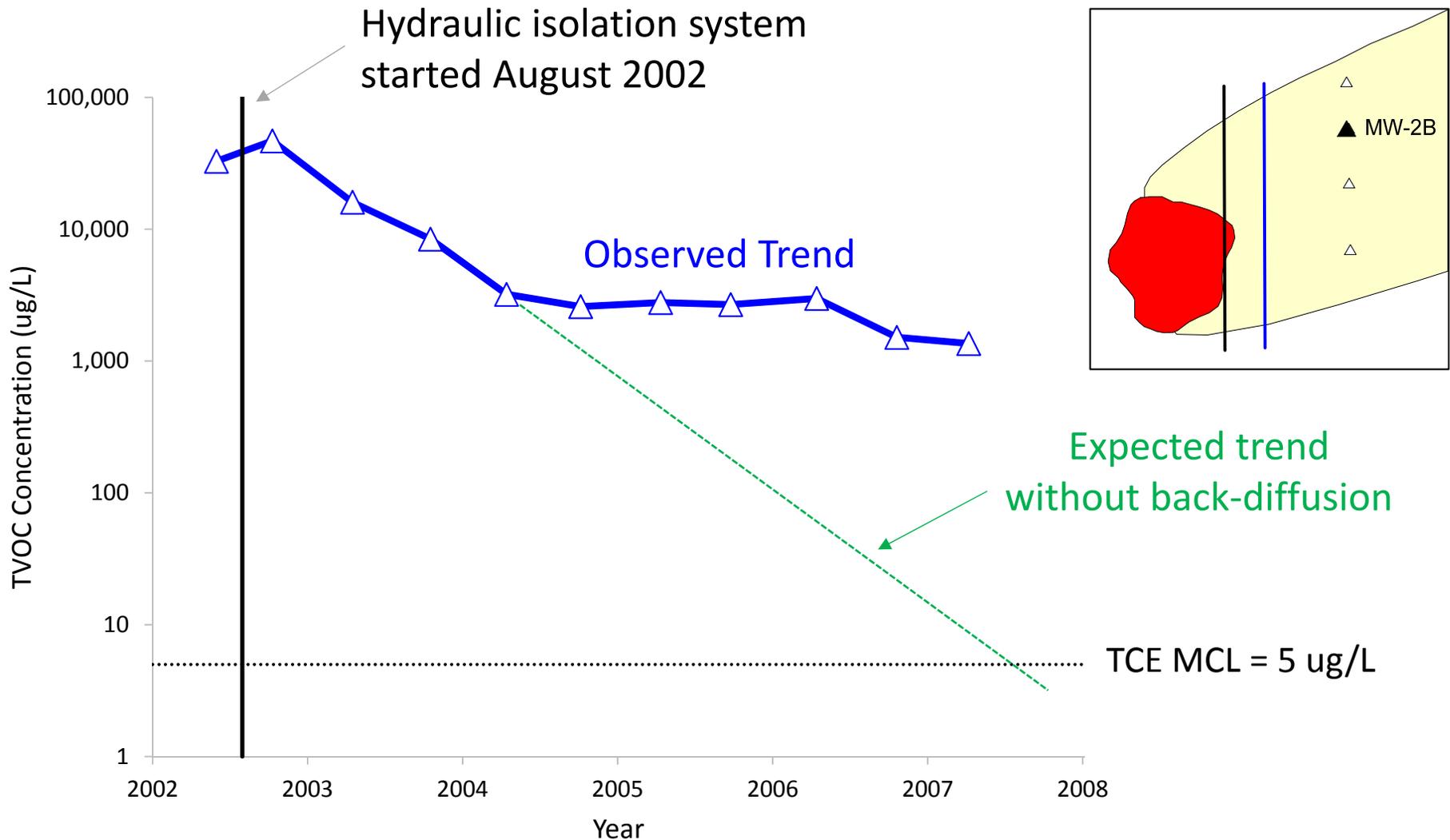
Rick McGregor

Application of an Adapted Version of
MT3DMS for Modeling Back-Diffusion
Remediation Timeframes

REMEDATION Autumn 2015

ISRM 2015 Local Domain Approach

TVOC Trend After Source Containment

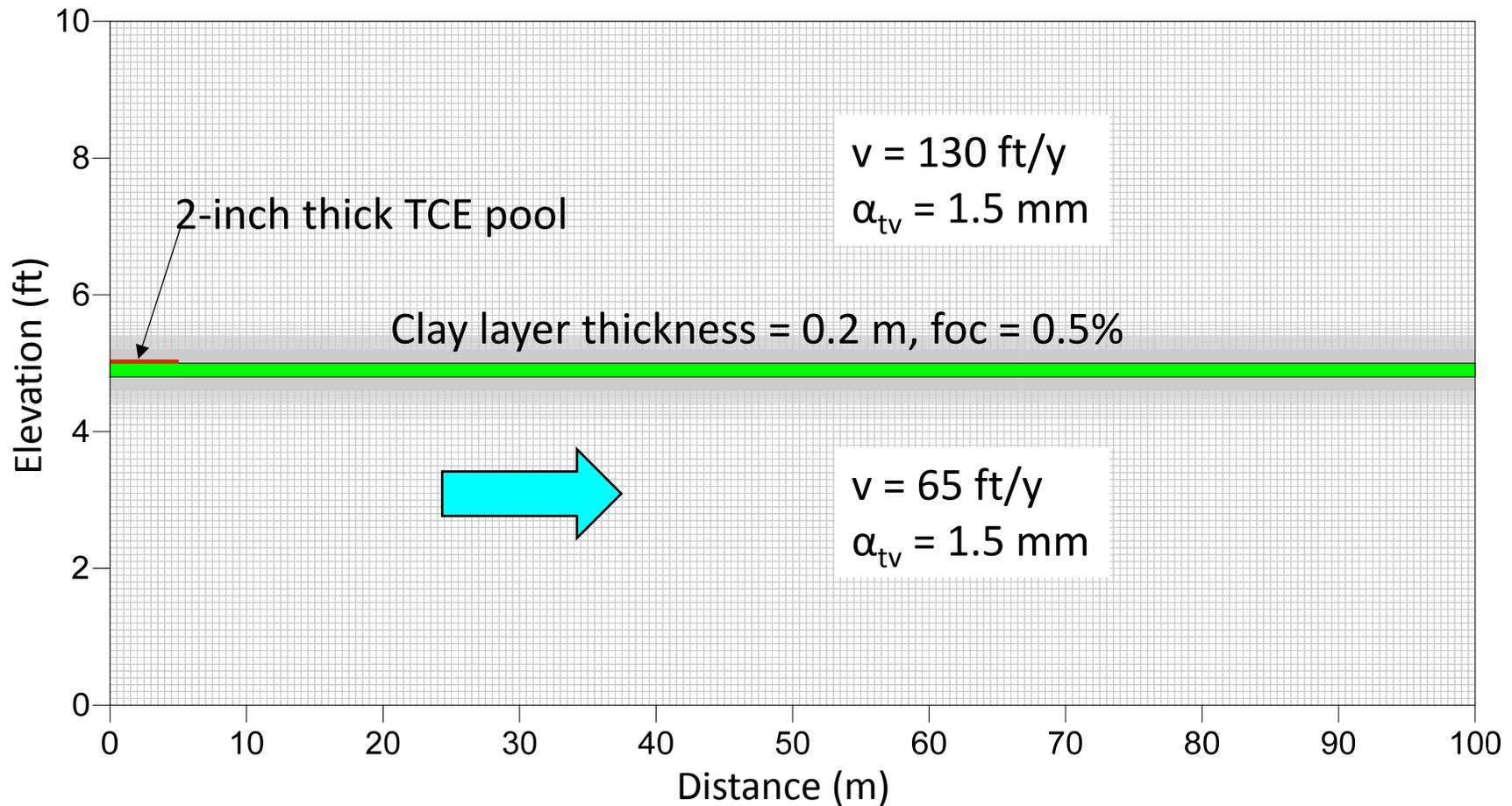


2-D Model Grid

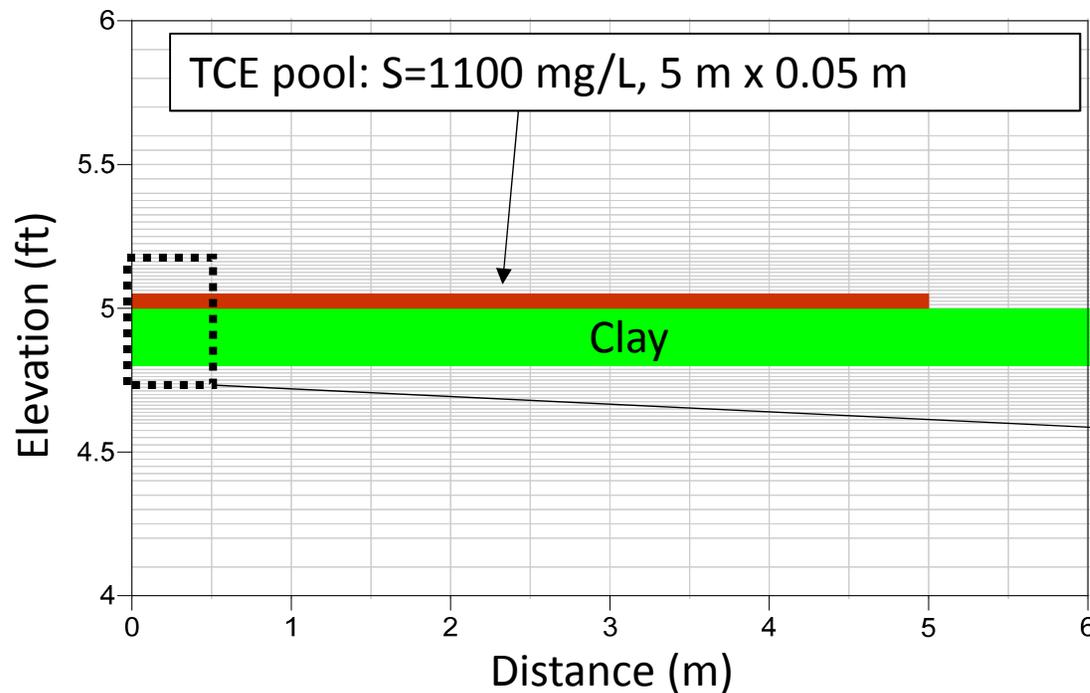
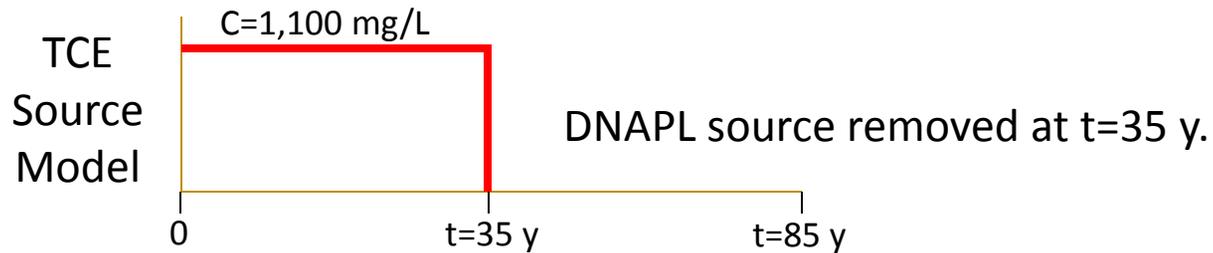
200 columns, 158 rows (layers)

Minimum grid spacing: $\Delta z = 1.25$ cm, $\Delta x = 0.5$ m

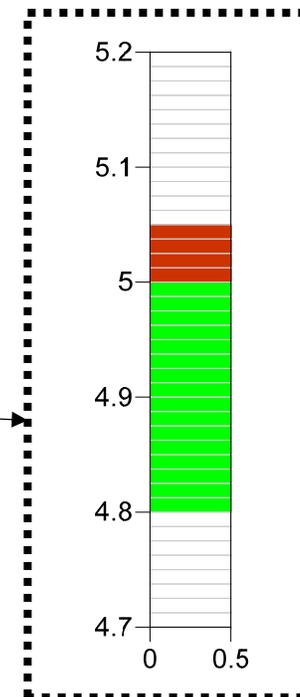
Run-time = 45 minutes for 85-y simulation ($\Delta t = 0.24$ d)



Source Characteristics

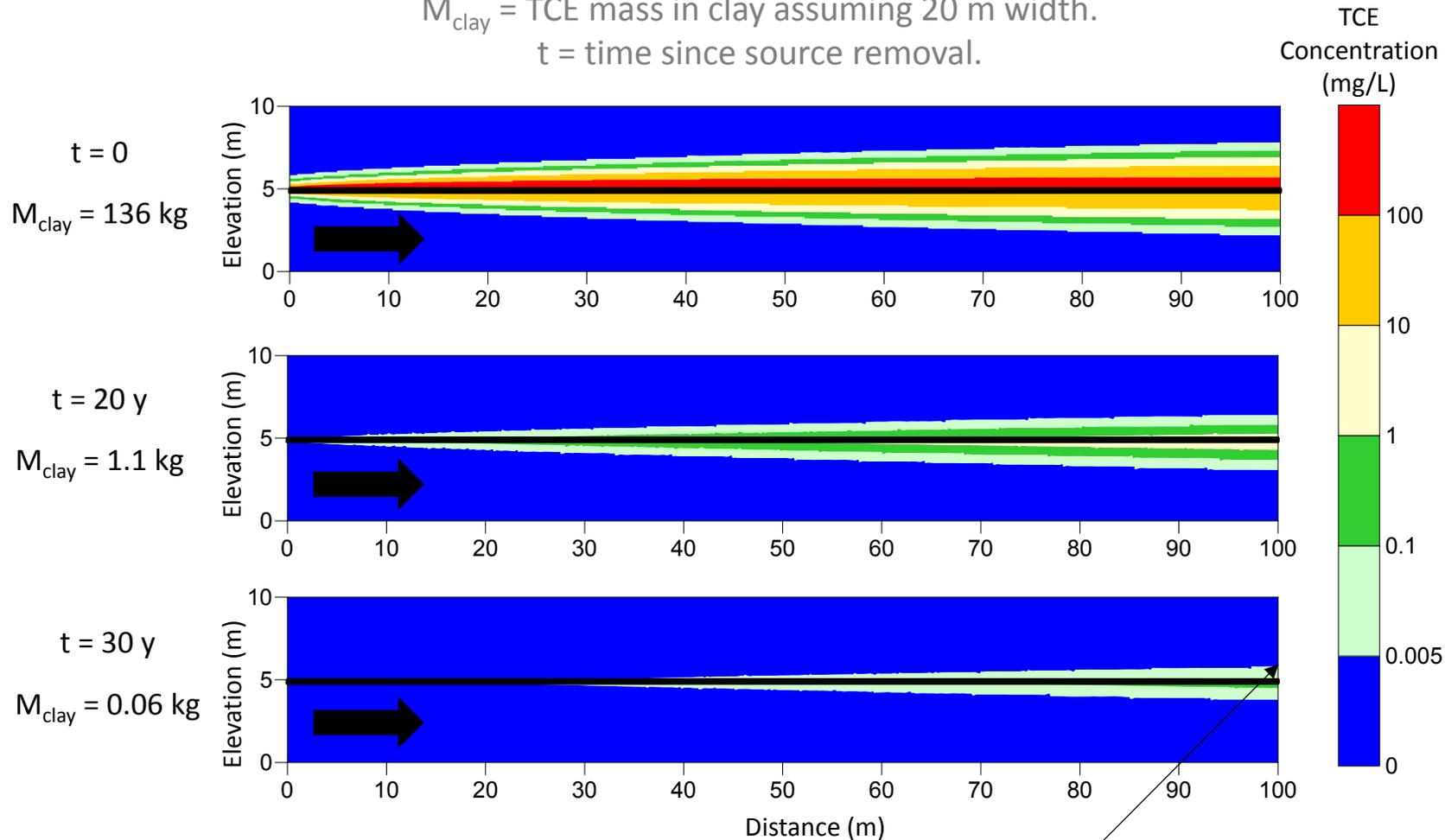


16 layers
in clay



Simulated TCE After Source Removal

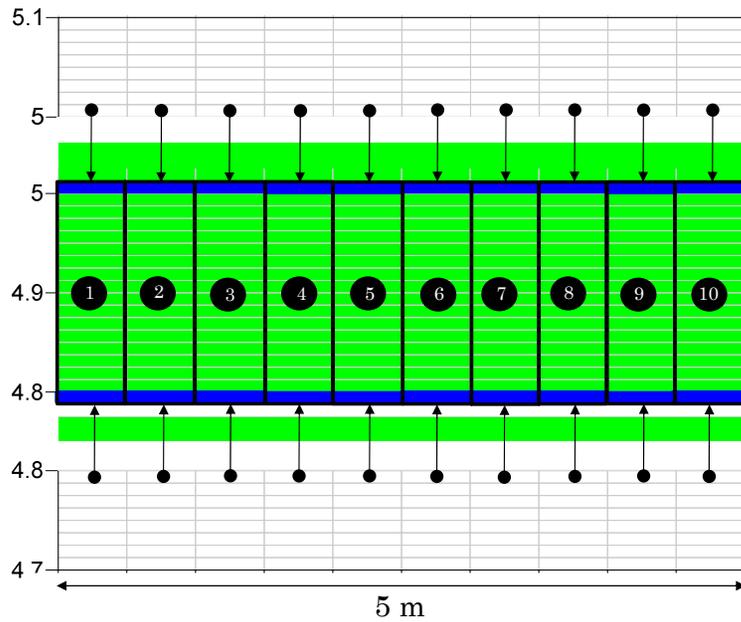
M_{clay} = TCE mass in clay assuming 20 m width.
 t = time since source removal.



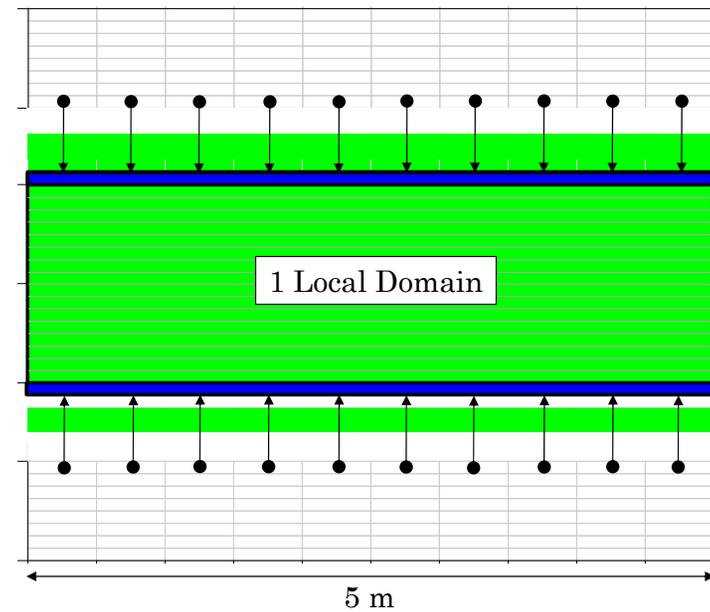
30 years after source removal:
 99.96% mass depletion in clay, avg. $C_{\text{well}} = 12 \text{ to } 126 \text{ ug/L}$

Carey et al. (2015)

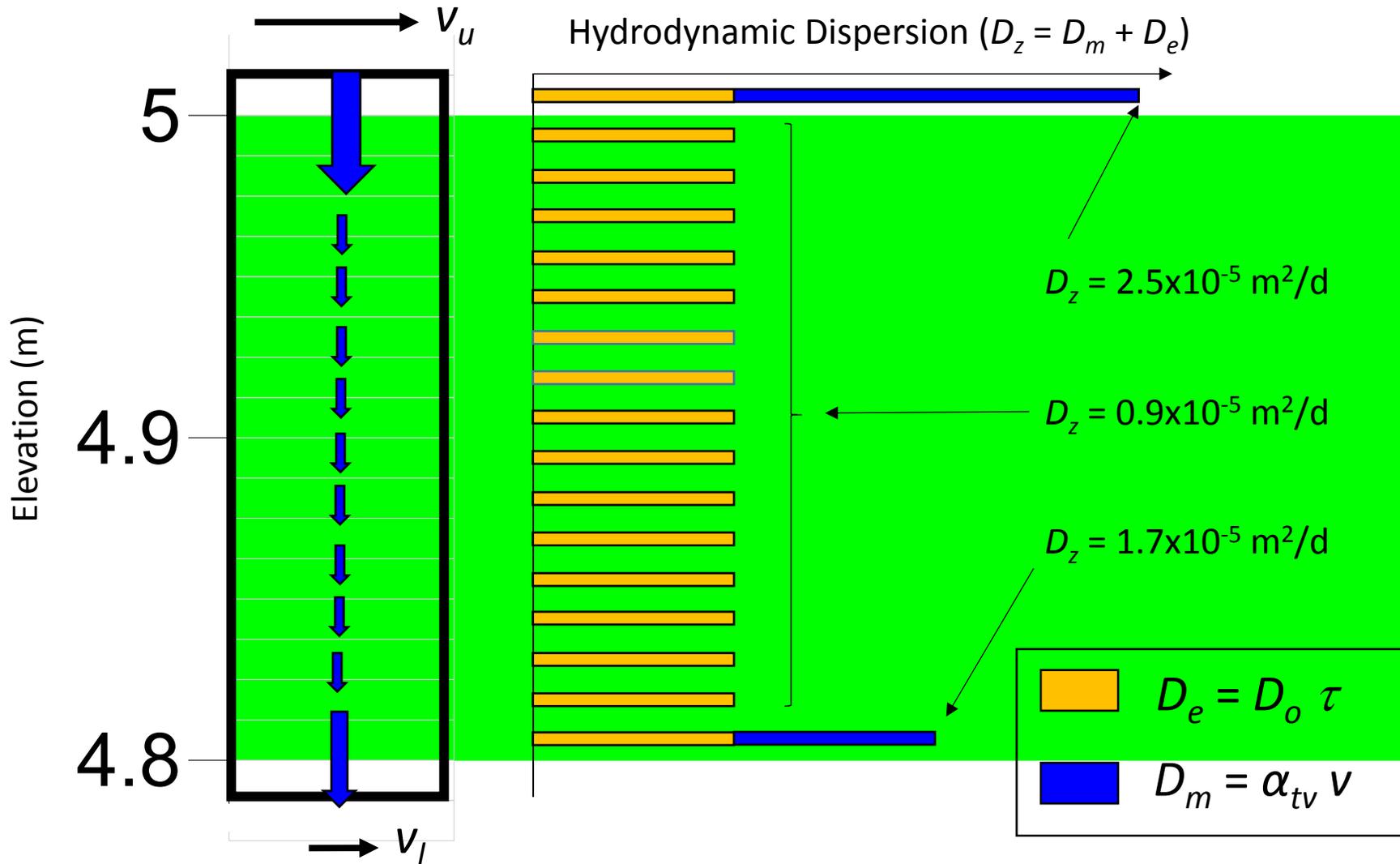
(a) Local domain models with $\Delta x_{LD} = 0.5$ m



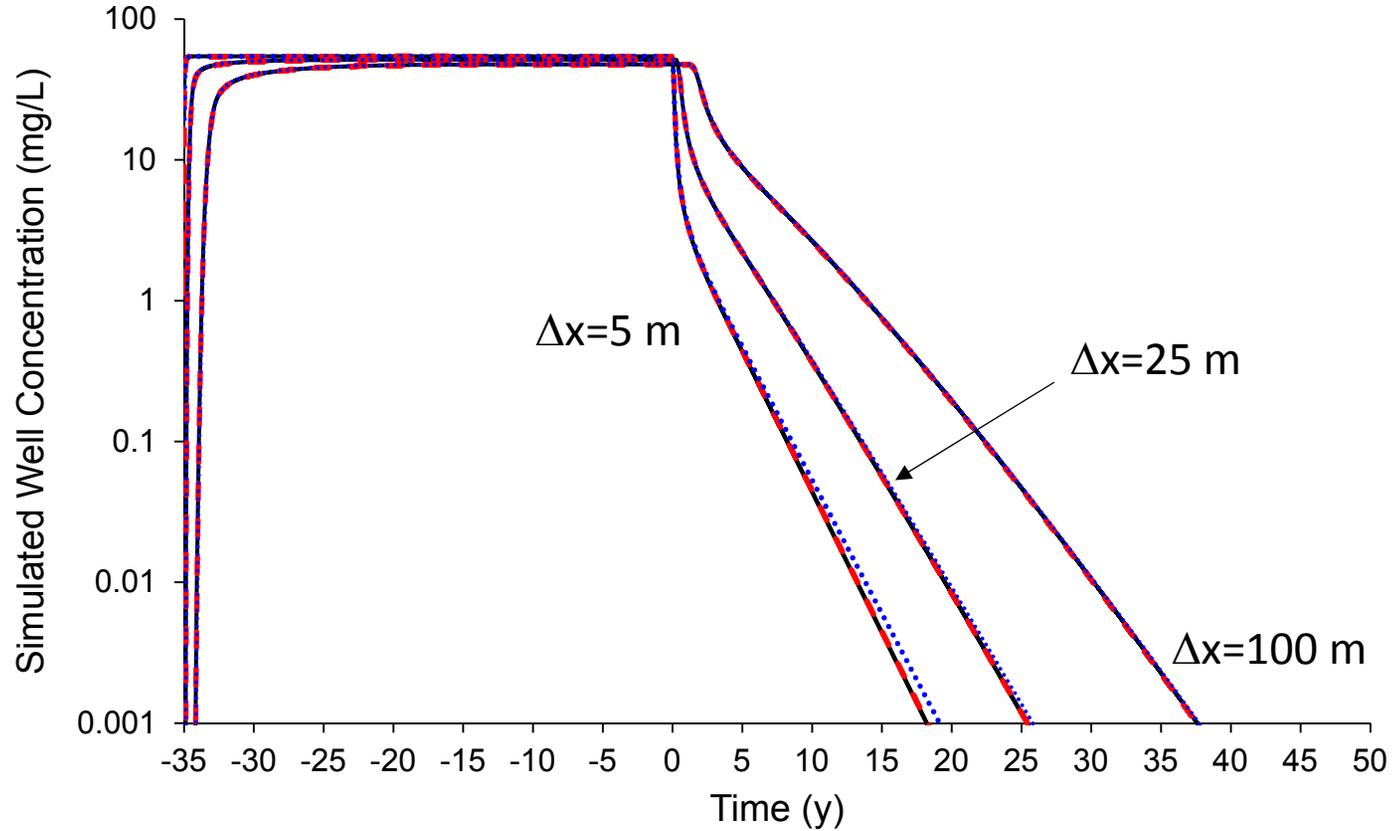
(b) Local domain models with $\Delta x_{LD} = 5$ m



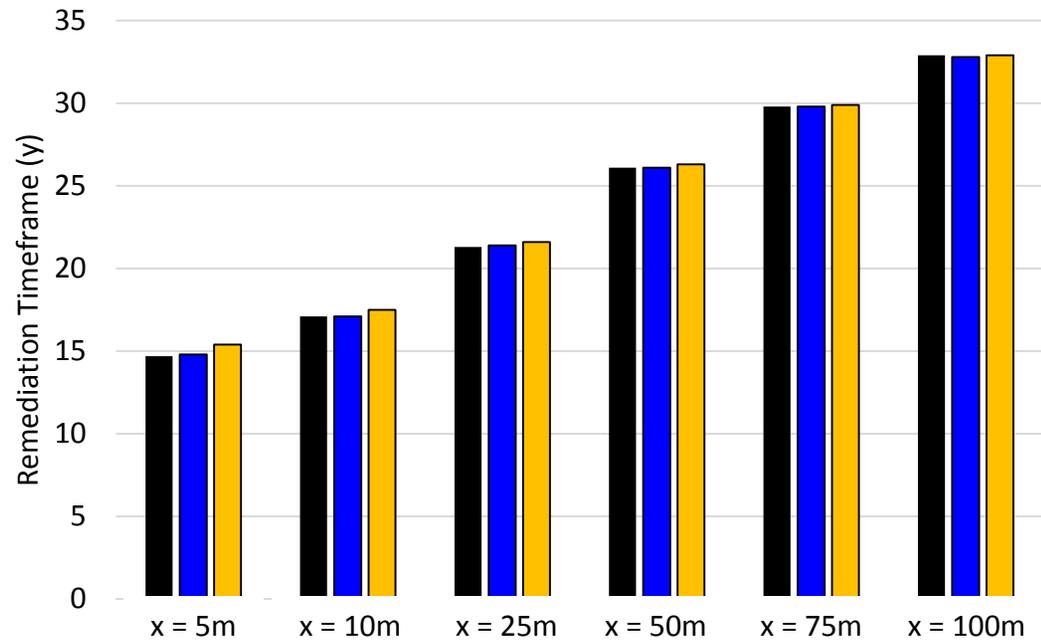
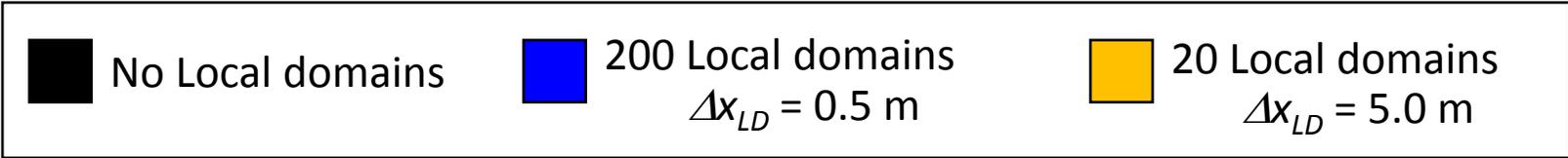
Conceptual illustration of local domains for two cases: (a) global and local domains have the same horizontal spacing; and (b) local domain has a larger horizontal spacing than the global domain grid.



Comparison of vertical mechanical dispersion (D_m) and effective diffusion coefficient (D_e) magnitudes in each grid cell of a 1-D local domain. Vertical mechanical dispersion is shown to be significant at the top and bottom clay-sand interfaces due to the use of a three-dimensional dispersion tensor and horizontal velocity components at each clay-sand interface. Application of a 1-D diffusion model will result in underestimation of the mass flux between the transmissive zone and clay layer.

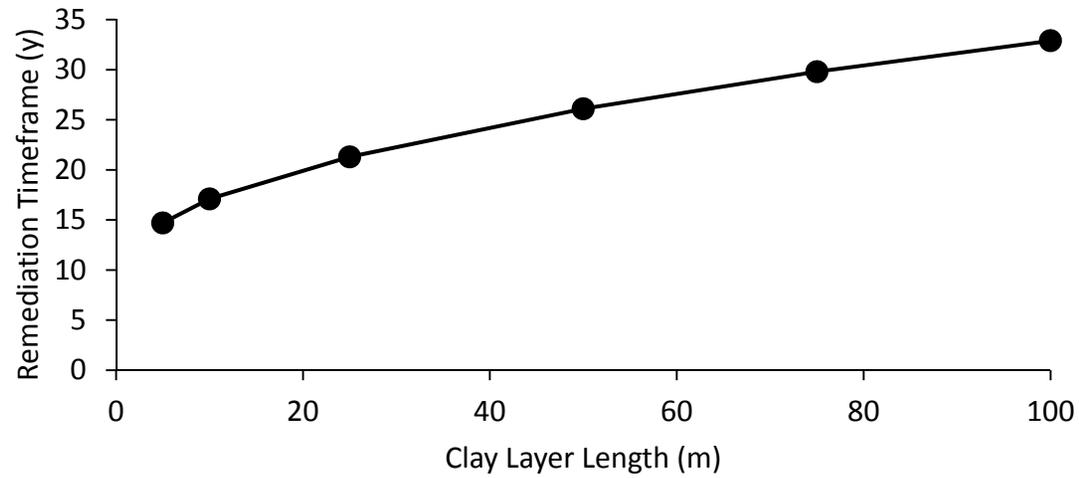


Simulated monitoring well concentrations at $x=5, 25,$ and 100 m. Solid lines represent the global domain model, dashed lines represent the local domain model with local grid $\Delta x=0.5$ m, and dotted lines represent the local domain model with local grid $\Delta x=5.0$ m.

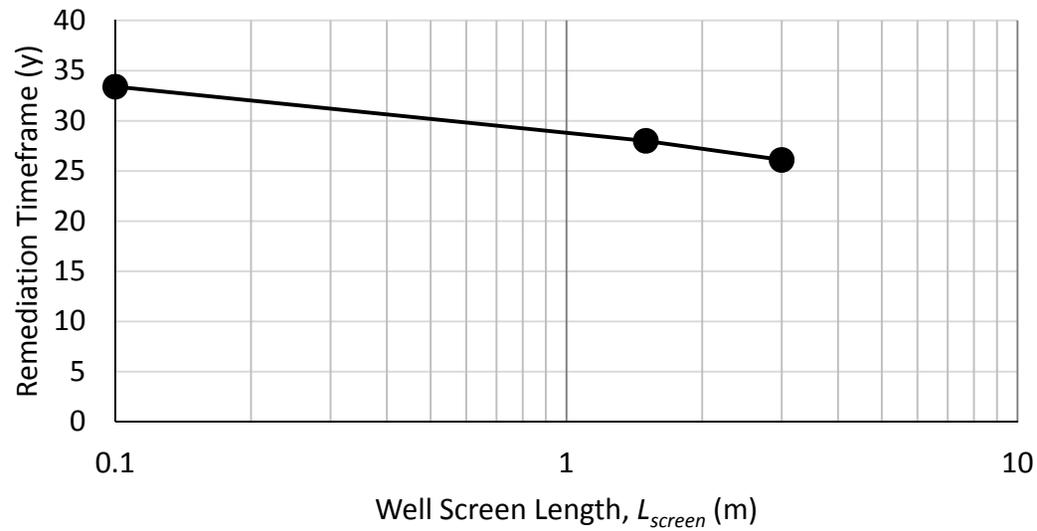


Simulated remediation timeframe for three model cases: (a) no local domains are used; (b) 200 local domains are used with horizontal spacing of 0.5 m; and (c) 20 local domains are used with horizontal spacing of 5.0 m. Based on monitoring well with $L_{screen} = 3$ m.

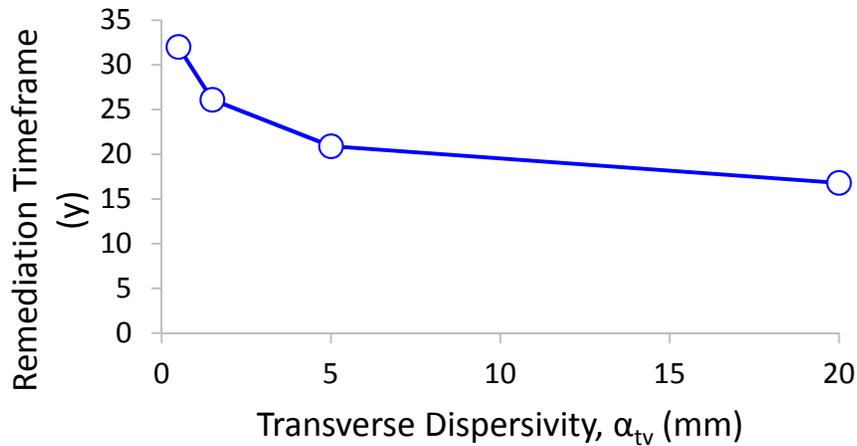
(a) Remediation timeframe versus clay layer length ($L_{screen}=3$ m)



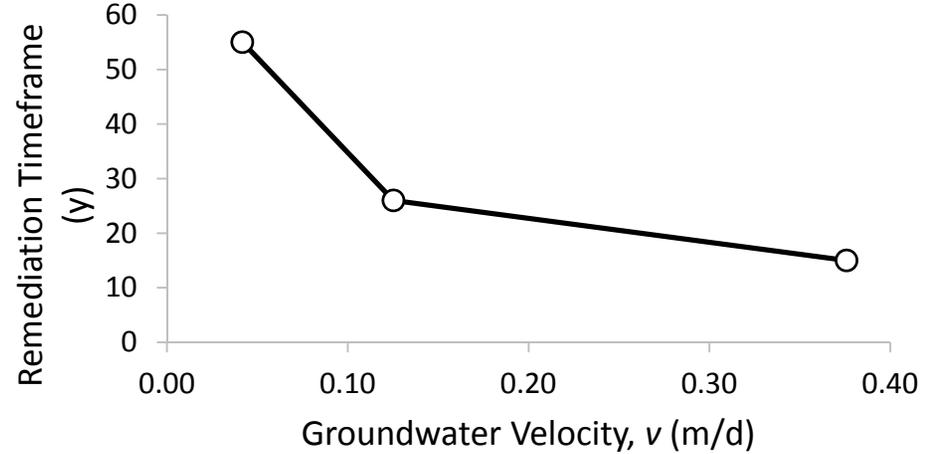
(b) Remediation timeframe versus well screen length ($x = 50$ m)



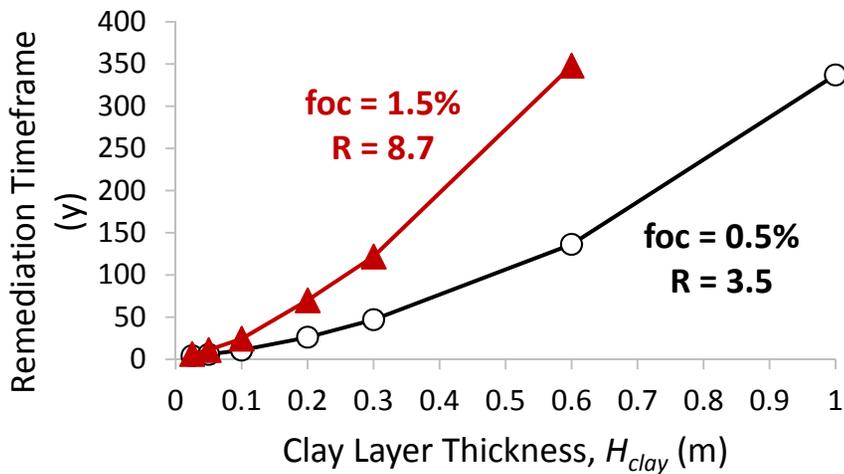
(a) Remediation timeframe versus α_{tv} .



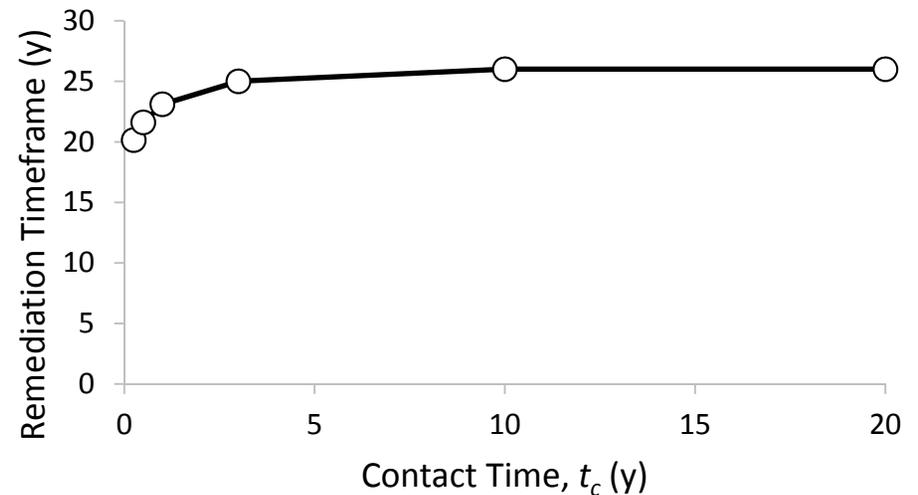
(c) Remediation timeframe versus v .



(b) Remediation timeframe versus clay layer thickness (H_{clay}).



(d) Remediation timeframe versus contact time between DNAPL and clay aquitard.



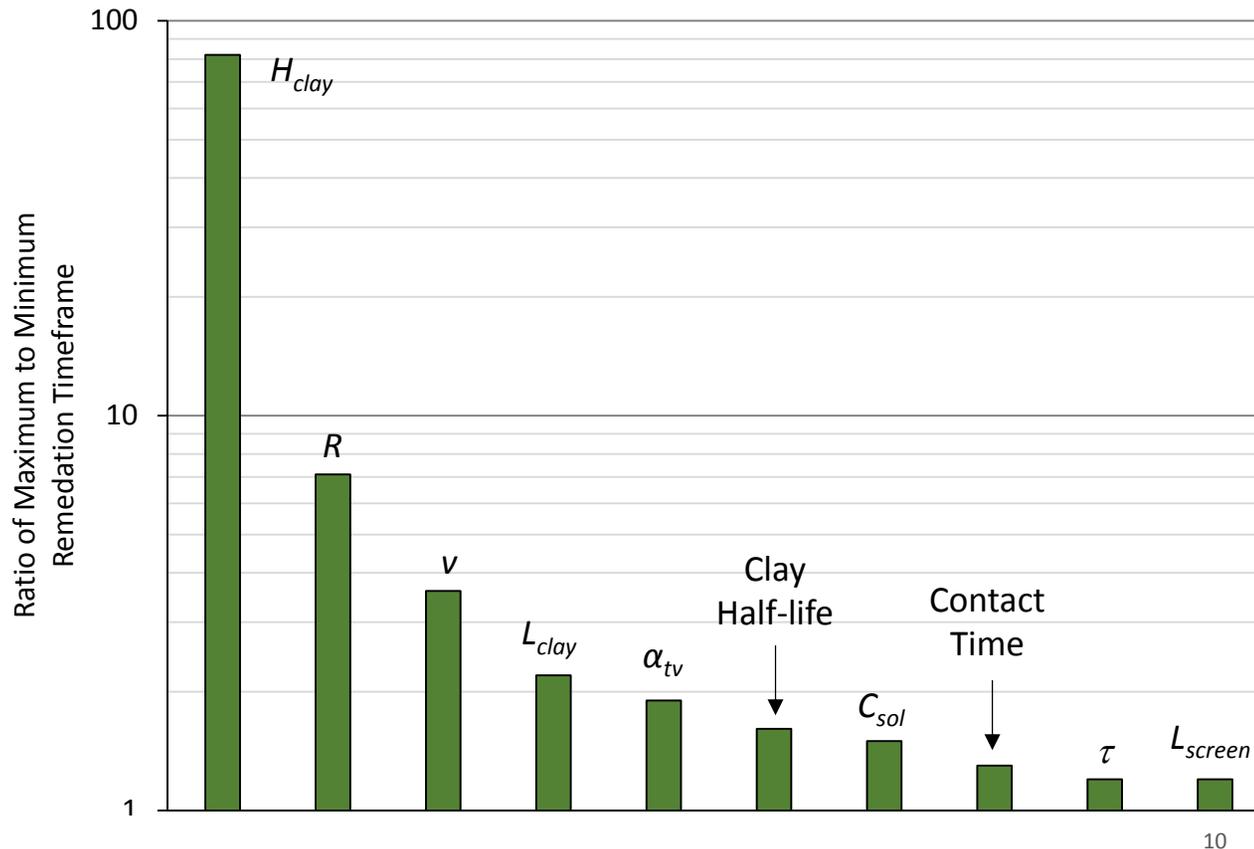


Exhibit 14 – Comparison of relative sensitivity of remediation timeframe to various input parameters, based on the ratio of maximum to minimum timeframe for each set of modeled parameter adjustments. H_{clay} is the clay layer thickness, R is the retardation coefficient, v is groundwater velocity, L_{clay} is the length of the clay layer, C_{sol} is solubility, τ is the tortuosity coefficient, and L_{screen} is the monitoring well screen length. Based on clay layer length of 50 m and well screen length of 3 m unless except for L_{clay} and L_{screen} parameter adjustments.